## RED ROCK CONSULTING

# Report of Geotechnical Investigation

CUT ANALYSIS – WEST PHASE 1 SH 29 STEPHENS COUNTY, OKLAHOMA

29657(10)

#### Prepared For:

**SRB** 

100 Northeast 5<sup>th</sup> Street Oklahoma City, Oklahoma 73104 Attention: Mr. Greg Allen, PE

#### Prepared By:

Red Rock Consulting, LLC PO Box 30591 Edmond, Oklahoma 73003 (405) 562-3328

> September 6, 2018 Project No. 18043



September 6, 2018

SRB

100 Northeast 5<sup>th</sup> Street Oklahoma City, Oklahoma 73104

Attention:

Mr. Greg Allen, PE

Re:

Report of Geotechnical Investigation
SH 29 Cut Analysis – West Phase 1

Stephens County, Oklahoma

29657(10)

Project No. 18043

Dear Mr. Allen:

I am pleased to submit herewith this report entitled "Geotechnical Investigation, SH 29 Cut Analysis – West Phase 1, Stephens County, Oklahoma, 29657(10)".

In an effort to provide a more environmentally friendly service, this report has been provided electronically. If you wish to receive a hard copy of this report, please contact our office.

It has been our pleasure to assist you with this project. Should you have any questions regarding the contents of this report, please contact Red Rock Consulting.

Yours very truly,

**RED ROCK CONSULTING, LLC** 

CA No. 5707 Exp. 06/30/19

Spencer Harris

**Project Specialist** 

Jeremy Basler, PE

Oklahoma PE No. 20233

#### REPORT OF GEOTECHNICAL INVESTIGATION

#### SH 29 CUT ANALYSIS - WEST PHASE 1 STEPHENS COUNTY, OKLAHOMA

#### 29657(10)

#### **PROJECT NO. 18043**

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#### REPORT OF GEOTECHNICAL INVESTIGATION

#### SH 29 CUT ANALYSIS – WEST PHASE 1 STEPHENS COUNTY, OKLAHOMA

29657(10)

#### **PROJECT NO. 18043**

#### INTRODUCTION

#### General

This report presents the results of the geotechnical investigation performed for the cut analysis associated with the offset alignment of SH 29 through Stephens County, Oklahoma. The purpose of this investigation is to evaluate the subsurface conditions at the site and to provide information pertaining to the geotechnical aspects of the proposed project.

#### **Proposed Construction**

The approximate 5.44-mile-long project consists of the construction of a new roadway on an offset alignment from 11.48 miles east of US 81 extending east 5.44 miles in Stephens County, Oklahoma. This report focuses on the cut sections required for the construction of the project.

For phase 1, four out of the seven significant cut sections that will be required to construct the proposed project are discussed in this report. The remaining three cut sections will be performed at a later date once ODOT acquires the properties. The first cut section, which includes CW-1 and CW-2, will be approximately 900 feet long between stations 652+00 to 661+00. The maximum proposed cut depth is 17 feet at station 654+00. The second cut section, which includes CW-3 and CW-4, will be approximately 860 feet long between stations 674+00 to 682+59. The maximum proposed cut depth is 15 feet at station 682+59. The third cut section, which includes CW-5, CW-6 and CW-7, will be approximately 900 feet long between stations 767+00 to 776+17. The maximum proposed cut depth is 32 feet at station 772+00. The fourth cut section, which includes CW-8 and CW-9, will be approximately 1200 feet long between stations 842+00 to 854+00. The maximum proposed cut depth is 17 feet at station 847+00. The first, third and fourth cut sections are to accommodate the proposed offset alignment. The second cut section is for an expanded drainage area to the south of the existing roadway.

#### Scope of Work

The scope of this investigation includes the following:

- Review of previous geotechnical and geological information of sites near this site. This was augmented with data obtained during the field investigation phase of the project.
- 2. Investigation of the subsurface soils by drilling and testing a total of 9 boreholes within the planned project area
- 3. A laboratory testing program consisting of moisture content, Atterberg limits, and sieve analysis on representative samples of the overburden soils
- 4. Rippability analysis of the bedrock encountered within the proposed cut depths

#### FIELD AND LABORATORY INVESTIGATIONS

#### Field Exploration

Subsurface exploration was performed on May 16 and July 11 - July 13, 2018. The borings were located in the field by a representative of Red Rock Consulting by measuring distances from known site reference points as depicted on plans provided by SRB. The locations of the borings should be considered accurate only to the degree implied by the methods used to define them.

The subsurface exploration program consisted of drilling 9 borings under the full-time supervision of a geologist. The borings are shown on the Boring Location Diagrams, which are included in Appendix A.

The borings were advanced with solid stem augers in all borings except CW-6, which was advanced using wet rotary drilling methods. All borings were advanced to depths approximately equal to 10 feet below the maximum anticipated cut depth using an all-terrain vehicle (ATV) mounted CME-750 drill rig equipped with an automatic hammer. The approximate cut and boring depths are summarized in Table 1.

Table 1 - Cut & Boring Depths

Boring	Station	CRL Offset	Proposed Cut Depth	Boring Depth
		(feet)	(feet)	(feet)
CW-1	654+00	50 left	17	30
CW-2	656+00	50 left	16	25
CW-3	676+00	50 left	14	25
CW-4	682+59	95 left	15	25
CW-5	770+00	50 left	20	30
CW-6	772+00	50 left	32	45
CW-7	774+00	50 left	20	30
CW-8	847+00	55 right	17	30
CW-9	849+00	50 right	13	25

Samples of the overburden materials were obtained in the borings as per Oklahoma Department of Transportation (ODOT) specifications. Representative samples of the overburden materials were obtained from the split-barrel sampler used for the standard penetration test (SPT) in general accordance with ASTM Specifications D-1586. After SPT refusal was attained, the hardness of bedrock was evaluated using a Texas Cone Penetrometer (TCP). The TCP was used in accordance with the AASHTO Manual on Subsurface Investigation and as modified by the Oklahoma Department of

Transportation. The sampling procedures are presented on the Boring Logs in Appendix A.

The SPT test uses a standard, 2-inch outside diameter, split-barrel sampling spoon that is driven into the bottom of the boring with a 140-pound automatic drive hammer that falls 30 inches. The blows per foot, N, is the number of hammer blows required to advance the sampling spoon the last 12 inches, or less, of an 18-inch sampling interval. The N value is used to estimate the in-situ relative density of granular soils, the consistency of cohesive soils, and the hardness of weathered bedrock.

The TCP test is a standard test developed by the Texas Highway Department to evaluate the consistency or hardness of the bedrock material. The TCP test drives a penetrometer cone into the bedrock material with a 140-pound automatic drive hammer that falls 30 inches. The TCP is driven for a series of blows, the first 10 being seating blows, followed by two 50 blow counts. After 50 blows of the automatic hammer, the distance the TCP has advanced is measured and recorded. The distance the TCP is driven is used to estimate the hardness of bedrock.

After performing SPT and TCP tests, the holes were backfilled with grout and cuttings as required by the Oklahoma State Statutes for Geotechnical drilling.

Samples were collected and transported back to the lab for further classification and testing. The final boring logs were developed from the draft logs, observations and test results of the samples returned to the laboratory. The stratigraphic contacts indicated are only for the specific dates and locations reported, and therefore, are not necessarily representative of other locations and times. The boring logs, presenting conditions encountered at each location explored, are included in Appendix A.

#### **Laboratory Testing**

Representative soil samples were tested to refine the field classifications and evaluate physical properties of the soils which may affect the geotechnical aspects of project design and construction.

The laboratory testing program included the following:

- Moisture content (AASHTO T265 / ASTM D2216)
- Liquid limit and plastic limit (AASHTO T89 & T90 / ASTM D4318)
- Particle size analysis of soils (AASHTO T88 / ASTM D1140)

The results of the physical laboratory tests conducted are shown on the Boring Logs in Appendix A and are also included in Appendix B.

The above laboratory tests were performed in general accordance with applicable AASHTO or ASTM procedures, or generally accepted practice. It should be noted that reference to AASHTO or ASTM procedures does not imply that all cross-referenced procedures in AASHTO or ASTM standards have been used, or that all AASHTO or ASTM procedures used have been followed exactly. Only those AASHTO or ASTM procedures and/or portions of procedures, which, in the professional judgment of the geotechnical engineer of record for this report, are applicable, appropriate, and necessary for this project, have been used or followed.

#### SITE DESCRIPTION

#### **Surface Conditions**

At the time of the field investigation, SH 29 was a two-lane undivided asphalt surfaced highway in the project area. There were grass shoulders to each side of the roadway through the cut sections. All the cut sections included in this report had shallow ditches.

The first cut section, CW-1 and CW-2, was located on the north side of SH 29 in a grass and dirt covered pasture. The pasture was elevated approximately 10 feet above the existing roadway. The west side of the second cut section, CW-3, was located on the north side of SH 29 in a grass yard. The yard was approximately 5 feet above the existing roadway. The east side of the second cut section, CW-4, was located on the north side of SH 29 in a relatively dense wooded area. There was a dry creek running north and south approximately 40 feet to the east, then curving to the west of the boring approximately 40 feet to the north. The third cut section, CW-5, CW-6 and CW-7, was located on the north side of SH 29 on top of a hill. The hill had exposed rock outcrops near the existing roadway and was approximately 20 feet above the existing roadway. The area was a moderately dense wooded area with small patches of clearings. There was a 70-foot-wide clearing north of the boring locations running east and west for a pipeline. The fourth cut section, CW-8 and CW-9, was located south of SH 29 on the side of a hill covered in grass and dirt. The boring locations were approximately 10 feet above the existing roadway.

There were only two boring locations within ODOT right of way; CW-8 and CW-9. Landowner permission was required for access to the rest of the borings. Dozer work was needed to access CW-4.

The surfaces were relatively flat where the borings were drilled. The boring locations were dry at the time of the field investigation. The ATV drill rig did not have any trouble moving around the sites.

The surface elevations were estimated from plans provided by SRB. Based on the plans, the elevations of the borings ranged between 1141 and 1228 feet. The approximate elevation at each boring location is shown on the Boring Location Diagrams and on the Boring Logs in Appendix A.

#### Site Geology

The geology of the cut sections was researched using the "Division Seven Engineering Classification of Geological Materials", published by the Oklahoma Department of Transportation (ODOT) and the Geologic Map of the "Hydrologic Atlas 3, Reconnaissance of the Water Resources of the Ardmore and Sherman quadrangles, southern Oklahoma," by Donald L. Hart, Jr., published by the Oklahoma Geological Survey in cooperation with the U.S. Geological Survey, 1974 and 1983.

#### ODOT PUBLICATION

The ODOT publication indicates all of the cut sections are underlain by the **El Reno unit** (Per). The geologic deposit and unit are described therein as follows:

The El Reno unit consists of a heterogeneous mixture of sandstones, shale, siltstone, and siltstone conglomerate. In northeastern Stephens County, the lowermost 40 to 100 feet of the unit consists dominantly of sandstones which are coarse-grained, nearly white to buff, and moderately soft; but a few hard, massive sandstone beds up to six feet thick occur near the base of the unit. Northward, across Grady County, the sandstones of this lower section become red, progressively finer grained, and moderately hard to hard.

The upper portion of the unit is known as "The Purple Series" in Stephens and Grady Counties. Here, some 80 feet of soft purple sandstone, 50 feet of soft pink sandstones, and 50 feet of moderately soft purple mudstone conglomerate are present in descending order. Westward, in Comanche and southern Caddo counties, the sandstones grade into red shales with minor amounts of gypsum and siltstones. Locally, in southeastern Grady County, near Cox City, a few sandstone beds in the upper portion are hard, limy, and occur in beds up to seven feet thick.

The unit thickens northward from 420 feet in Stephens County to 460 feet in Western Caddo County to 660 feet in northern Grady County.

The El Reno unit outcrops in a four to eight-mile-wide northwest-southeast band across southern Caddo, northeastern Comanche, and northwestern Stephens Counties. The outcrop then circles the southeastern end of the Anadarko basin in northern Stephens County and covers a broad area up to eighteen miles wide across northeastern Stephens and Grady Counties of Division 7. In Grady and eastern Caddo Counties, north of T4N, the upper 0 to 230 feet is mapped separately as the Dog Creek-Blaine subunits undifferentiated. Northward, in Division 4, and westward from Caddo County, in Division 5, the rock strata of the El Reno unit are separable and are mapped as the Flowerpot, Blaine, and Dog Creek units.

Topographically, the unit generally forms rolling hills with a pronounced escarpment at the base in Stephens and southern Grady Counties where the sandstones are thickest. Northwestward, the topography is rolling with gently rolling topography dominant in western Caddo County where the shales are thickest. The sandstone ridges are usually marked by oak vegetation and erosional gullies in the sandy soils. The shales generally form the valleys and gently rolling hills and support the growth of short grass. Some mesquite and prickly pear are evident in the salty or gypsiferous areas.

#### OKLAHOMA GEOLOGICAL SURVEY

According to the hydrologic atlas, all the cut sections are underlain by the **Duncan** Sandstone (Pd) of the Permian-aged El Reno Group. The geologic deposit and formation are described therein as follows:

Duncan Sandstone: **Sandstone**, white to buff, fine to coarse grained, **moderately indurated**, **with interbedded mudstone conglomerates and siltstone**; thickness, 100 to 400 feet, decreasing southeastward. Yields small to moderate amounts of water of fair quality.

#### **Subsurface Conditions**

Information collected during this investigation indicates that the overburden consisted of clays with varying amounts of sand and sands with varying amounts of silt and clay that extended from the surface to the top of bedrock in all borings. The overburden materials, including the sandstone rock, appeared to be native to the site.

The bedrock was the same in all the boring discussed in this report with slight variations in color. The color was observed as a light gray with reddish brown variations as shown on the Boring Logs in Appendix A. The approximate depths and types of bedrock are summarized in Table 2.

Table 2 – Depth & Type of Bedrock

Boring	Depth to Bedrock (feet)	Elevation (feet)	Туре
CW-1	0.5	1227.5	sandstone
CW-2	6	1220	sandstone
CW-3	10.5	1203.5	sandstone
CW-4	20	1171.5	sandstone
CW-5	6	1135	sandstone
CW-6	4.5	1150	sandstone
CW-7	5	1137.5	sandstone
CW-8	4	1171	sandstone
CW-9	4	1163	sandstone

The rippability of bedrock is discussed in the *Rippability of Bedrock* section of this report. Subsurface conditions are described in greater detail on the Boring Logs in Appendix A.

#### **Groundwater Conditions**

Groundwater conditions were monitored in the borings during and immediately following the completion of drilling activities. The approximate groundwater levels are summarized in Table 3. All the borings remained open (did not cave in) following drilling.

Table 3 - Groundwater Levels

_	During [	<u> Drilling</u>	After Dri	lling
Boring	Depth (feet)	Elevation (feet)	Depth (feet)	Elevation (feet)
CW-1	none	none	none	none
CW-2	none	none	none	none
CW-3	none	none	none	none
CW-4	23	1168.5	21	1170.5
CW-5	15	1126	16.5	1124.5
CW-6	none	none	None	None
CW-7	none	none	None	None
CW-8	10	1165	12	1163
CW-9	none	none	none	none

To obtain more accurate groundwater level information, long-term observations in a well or piezometer that is sealed from the influence of surface water would be needed. Fluctuations in groundwater levels can occur due to seasonal variations in the amount of rainfall, runoff, altered drainage paths, and other factors not evident at the time borings were advanced. Consequently, the contractor should be aware of these possibilities while constructing this project.

#### RIPPABILITY OF BEDROCK

Very poorly cemented to very well cemented sandstone bedrock was encountered in the borings and are summarized in Table 4. Difficulties in excavating due to the hardness of the bedrock generally are not anticipated for this project; however, there will likely be some areas that are non-rippable.

**Table 4 – Hardness of Bedrock Materials** 

Table 4 - Hardness of Dedrock Materials					
Boring	Depth to Bedrock (feet)	Elevation (feet)	Туре	TCP Value (in/100 blows)	Hardness
CW-1	0.5	1227.5	sandstone	6.8-7.1	very poorly cemented
	16	1212	sandstone	1.3	well cemented
	21	1207	sandstone	0.9	very well cemented
	26	1202	sandstone	1-1.1	well cemented
CW-2	6	1220	sandstone	8	very poorly cemented
	10	1216	sandstone	1-1.3	well cemented
CW-3	10.5	1203.5	sandstone	2.4	cemented
	15	1199	sandstone	2	well cemented
	20	1194	sandstone	0.8-0.9	very well cemented
CW-4	20	1171.5	sandstone	1.4	well cemented
	25.5	1166	sandstone	0.4	very well cemented
CW-5	6	1135	sandstone	5.1	poorly cemented
	10	1131	sandstone	2.8	cemented
	15	1126	sandstone	1.2	well cemented
	20	1121	sandstone	3.5	poorly cemented
	25	1116	sandstone	1.2-1.5	well cemented
CW-6	4.5	1150	sandstone	5	poorly cemented
	10	1144.5	sandstone	2.8	cemented
	15	1139.5	sandstone	0.5-0.8	very well cemented
	35	1129.5	sandstone	1.2-1.4	well cemented
CW-7	5	1137.5	sandstone	2.1	cemented
	10	1132.5	sandstone	1.3-1.8	well cemented
	20	1122.5	sandstone	2.5	cemented
	25	1117.5	sandstone	1.4	well cemented
	30	1112.5	sandstone	0.8	very well cemented
CW-8	4	1171	sandstone	2.1-2.3	cemented
	14.5	1160.5	sandstone	1.1-1.5	well cemented
CW-9	4	1163	sandstone	1.3-1.5	well cemented
	14.5	1152.5	sandstone	0.8	very well cemented
	19.5	1147.5	sandstone	2.3	cemented
	24.5	1142.5	sandstone	1.4	well cemented
	24.0	1144.0	อสเนอเบเษ	1.4	well celllellled

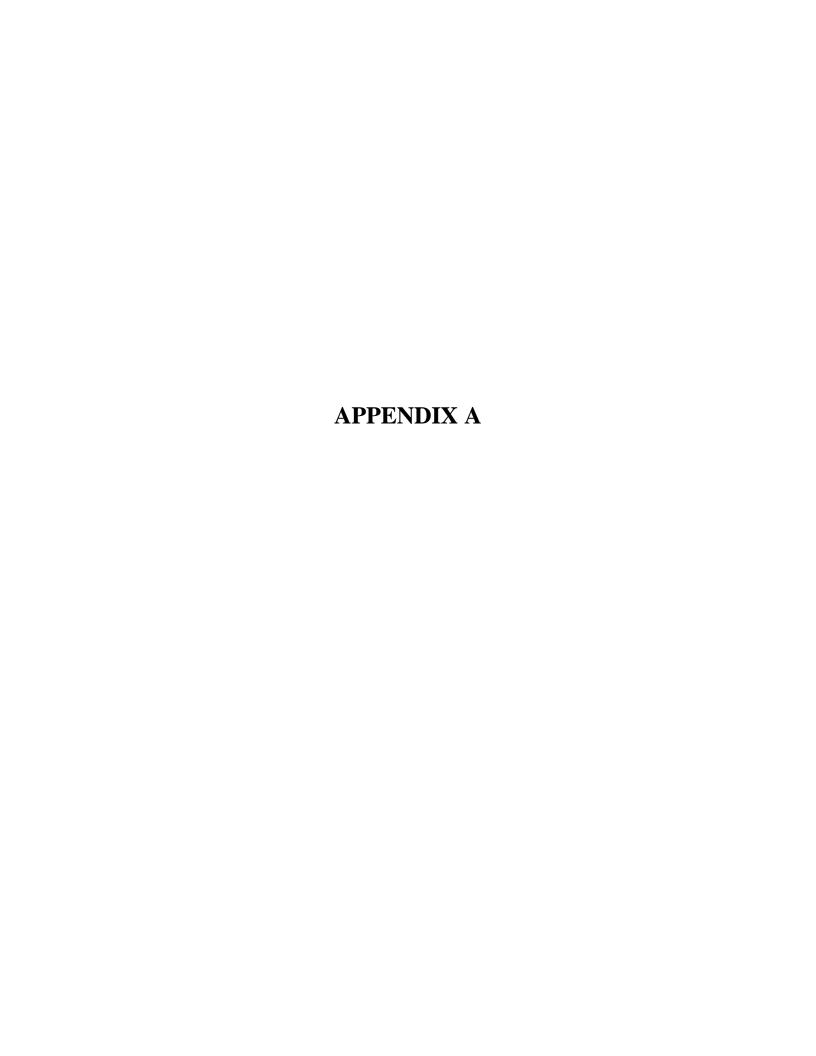
Generally, sedimentary rock which have a penetration of 2 inches or more per 100 blows of the Texas Cone Penetrometer (TCP) test can typically be excavated with normal excavating equipment. Most of the sandstone bedrock encountered in the proposed cut sections at this site that was tested for hardness falls into (or is very close to) the "rippable" category. The TCP tests that resulted in a penetration of less than 1 inch is assumed to be the massive basal sandstone mentioned below that is considered non-rippable. The non-rippable sandstone was mostly encountered below the proposed cut section depths, except for CW-6. A non-rippable section was observed between 15-35 feet as shown in table 4. Additional non-rippable areas will likely be encountered in the cut sections because hardness of bedrock can be variable between borings or in relatively short distances.

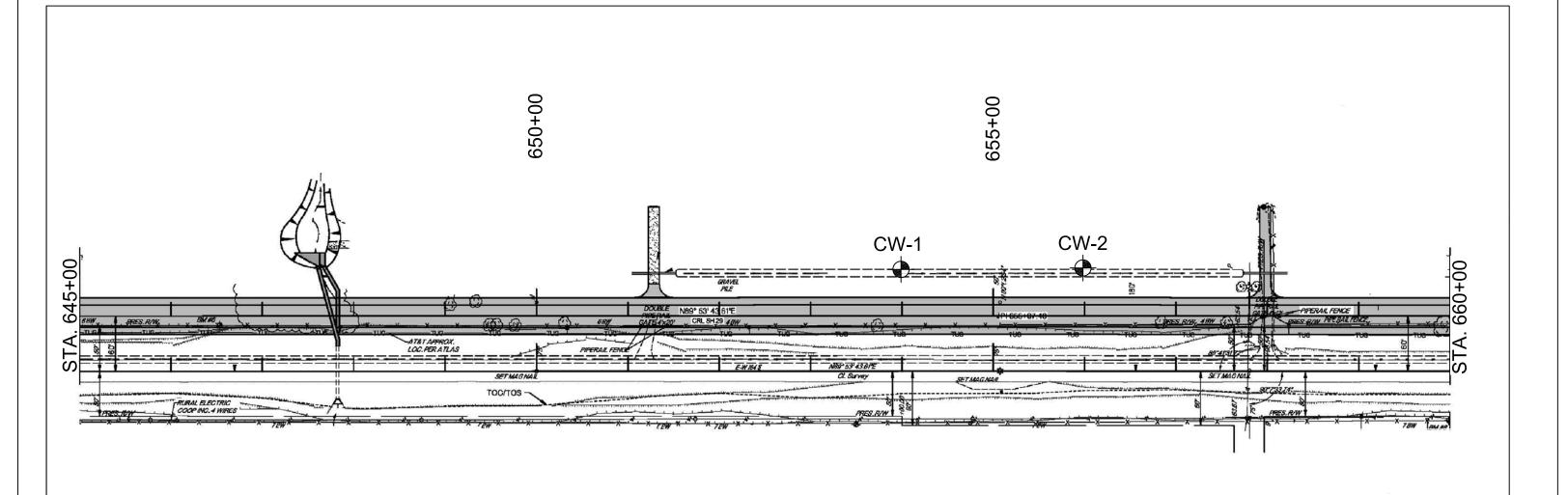
It should also be noted the "Engineering Classification of Geologic Materials" manual published by the Oklahoma Department of Transportation (ODOT) indicates that the apparent rippability of the bedrock materials (as defined for the El Reno geologic unit in Stephens County) is "generally rippable; six feet thick massive basal sandstone is non-rippable". The ODOT publication also defines rippability as the susceptibility of a rock to be broken by a ripping device as pulled by a Caterpillar D9 or its equivalent.

#### **CLOSURE**

The data presented in this report are based on the negotiated scope for this project and site conditions as they existed at the time of the field exploration. The conditions encountered in the exploratory borings are representative subsurface conditions within the study area.

This report was prepared for the exclusive use of SRB, ODOT and their agents and consultants. It should be made available to prospective contractors for information and factual data only and not as a warranty of subsurface conditions similar to those interpreted from the boring logs or discussions presented herein.





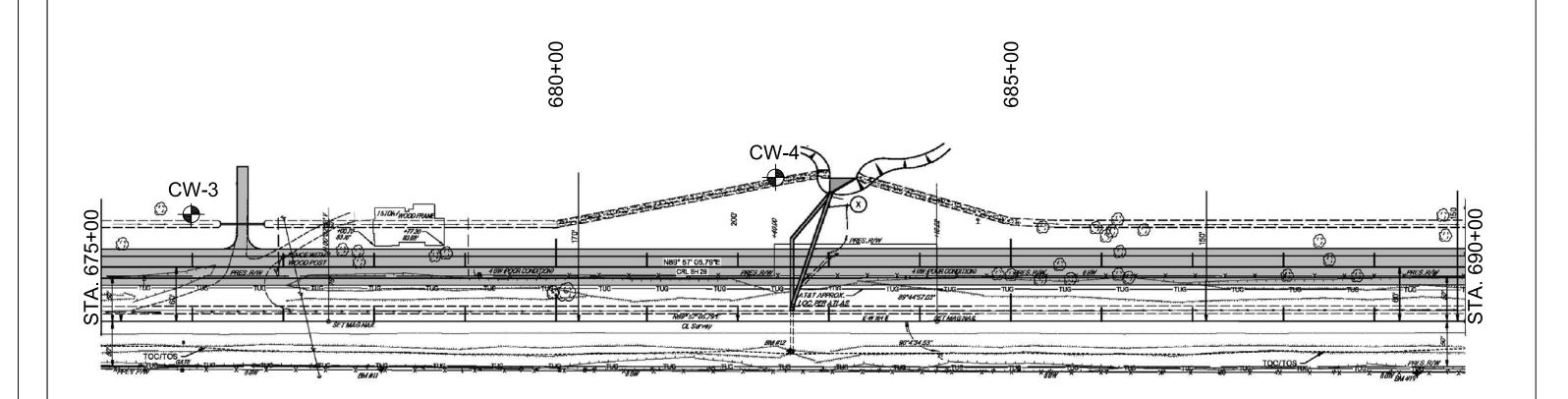
BORING LOCATIONS AND ELEVATIONS				
Boring Station CRL Offset Elevation				
CW-1	654+00	50' LT	1228'	
CW-2	656+00	50' LT	1226'	

### RED ROCK CONSULTING

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#### **BORING LOCATION DIAGRAM**

Project Mngr:	SAH	Project No. 18043
Designed By:	SAH	Scale: NOT TO SCALE
Checked By:	JWB	Date: 8/15/2018
Approved By:	JWB	Page No: 1/4



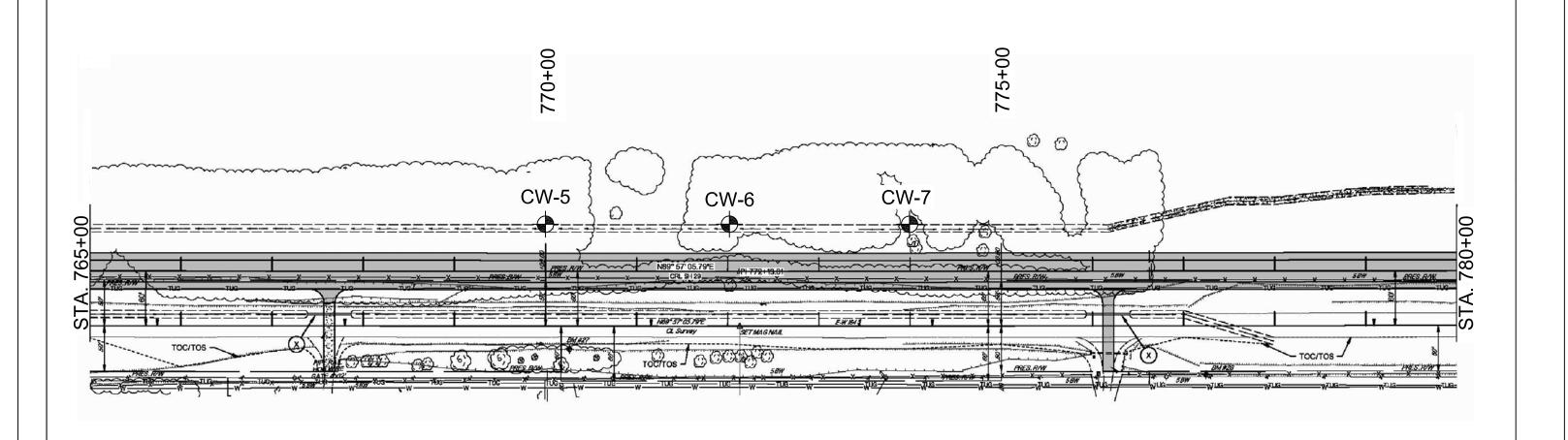
BORING LOCATIONS AND ELEVATIONS				
Boring	Station	CRL Offset	Elevation	
CW-3	676+00	50' LT	1214'	
CW-4	682+59	95' LT	1191.5'	



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BORING LOCATIONS AND ELEVATIONS				
Boring	Station	CRL Offset	Elevation	
CW-5	770+00	50' LT	1141'	
CW-6	772+00	50' LT	1154.5'	
CW-7	774+00	50' LT	1142.5'	

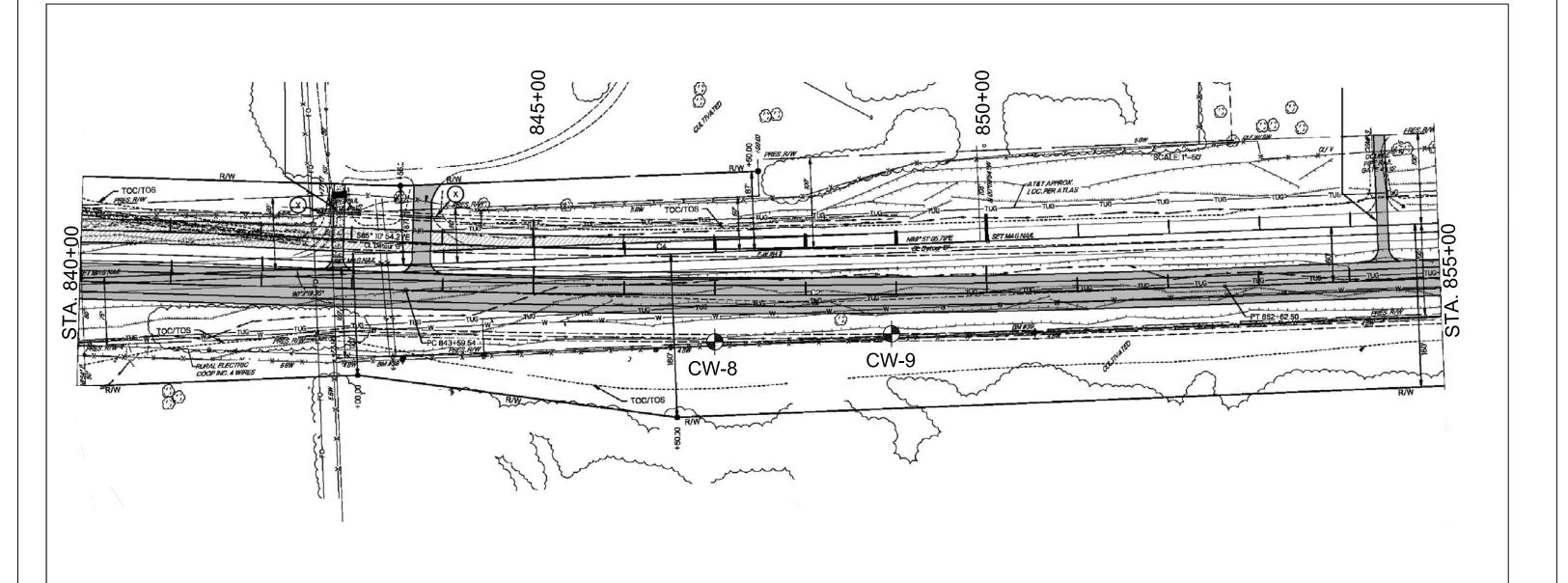


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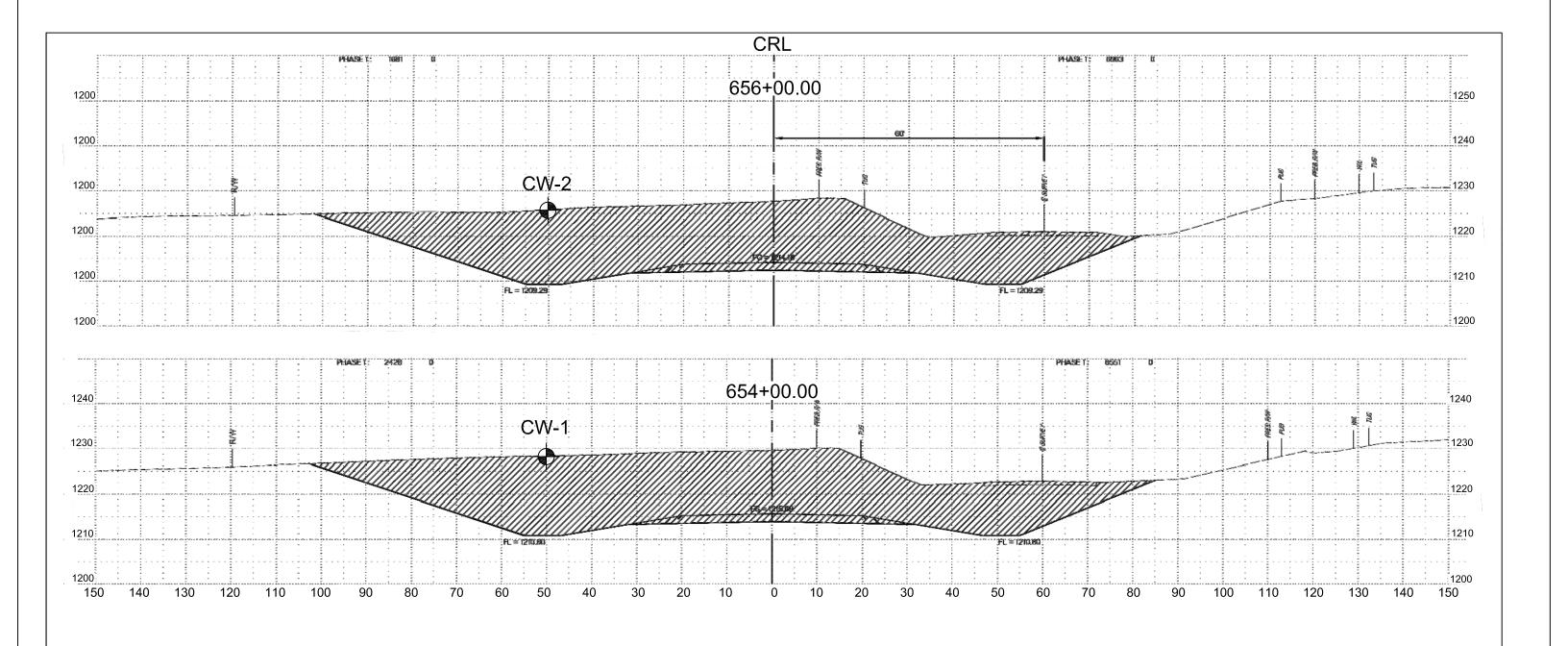
BORING LOCATIONS AND ELEVATIONS				
Boring	Station	CRL Offset	Elevation	
CW-8	847+00	55' RT	1175'	
CW-9	849+00	50' RT	1167'	

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#### **BORING LOCATION DIAGRAM**

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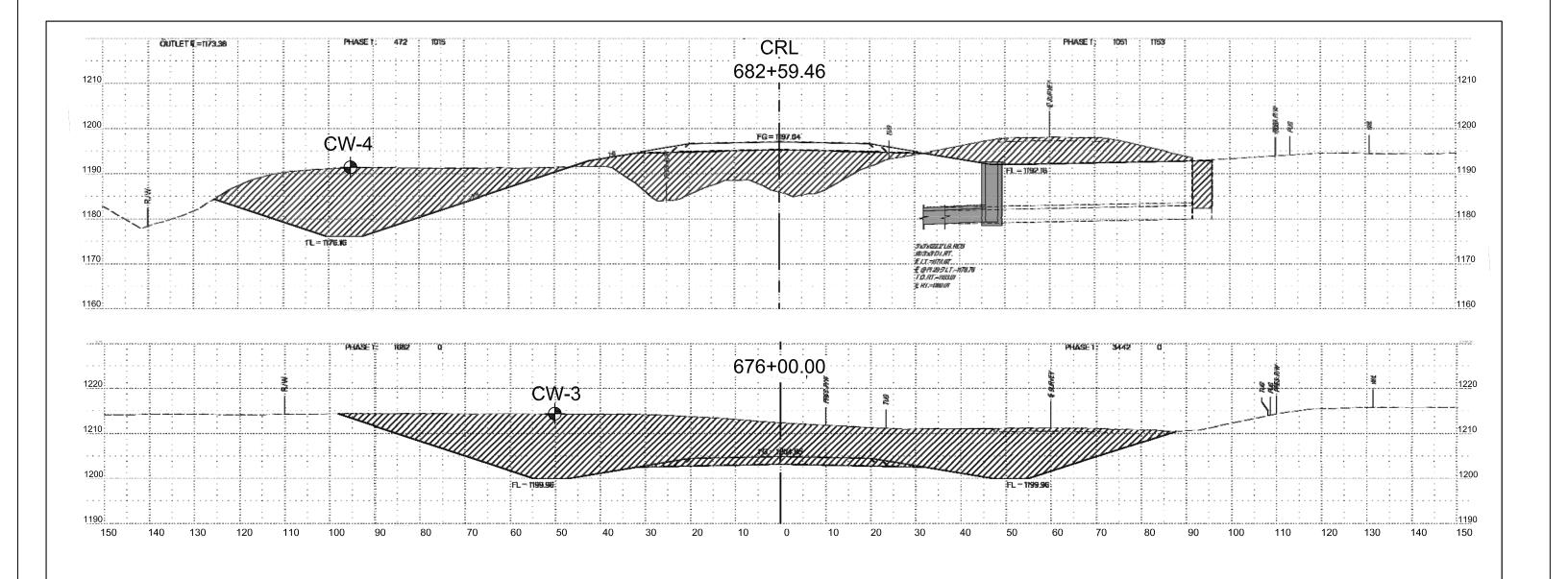
BORING LOCATIONS AND ELEVATIONS						
Boring	Station	CRL Offset	Elevation			
CW-1	654+00	50' LT	1228'			
CW-2	656+00	50' LT	1226'			

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#### BORING LOCATION DIAGRAM - CROSS SECTIONS

Project Mngr:	SAH	Project No. 18043				
Designed By:	SAH	Scale: NOT TO SCALE				
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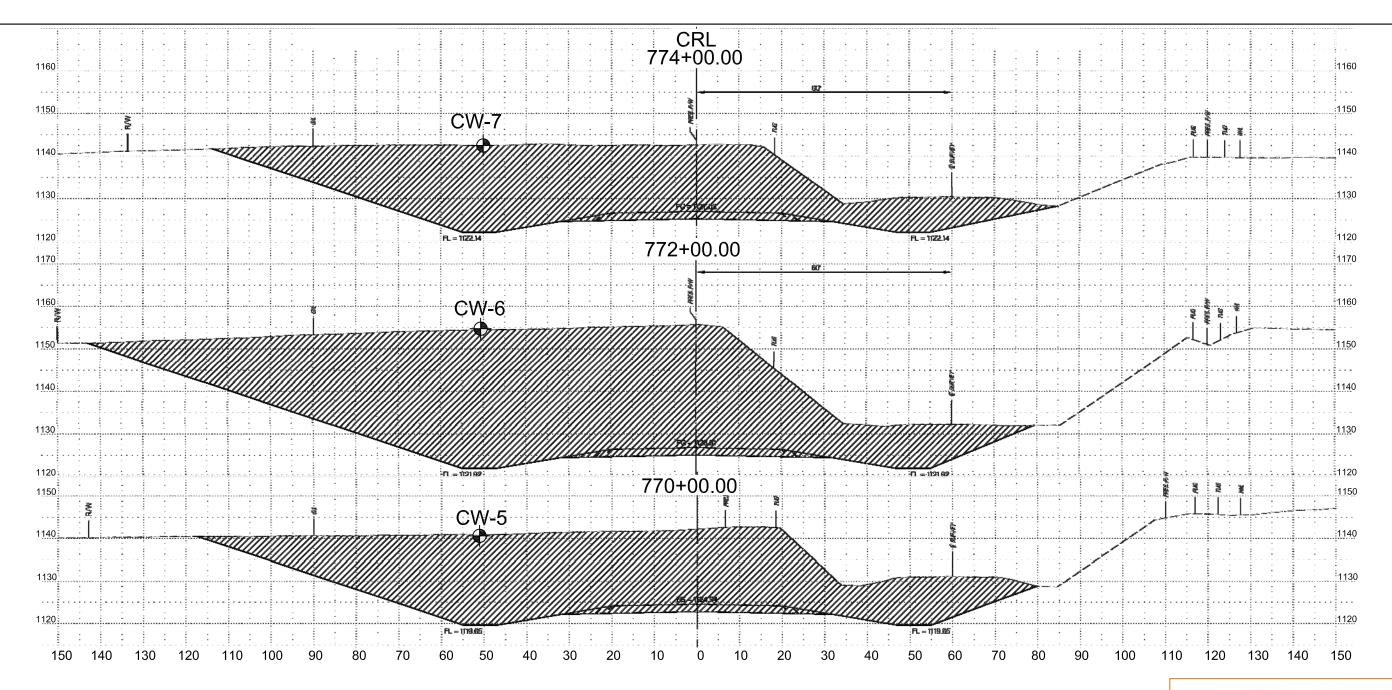
BORING LOCATIONS AND ELEVATIONS						
Boring	Elevation					
CW-3	676+00	50' Left	1214			
CW-4	682+59	95' Left	1191.5			

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#### BORING LOCATION DIAGRAM - CROSS SECTIONS

Project Mngr:	SAH	Project No.	18043
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Approved By:	JWB	Sheet No. 2	/4



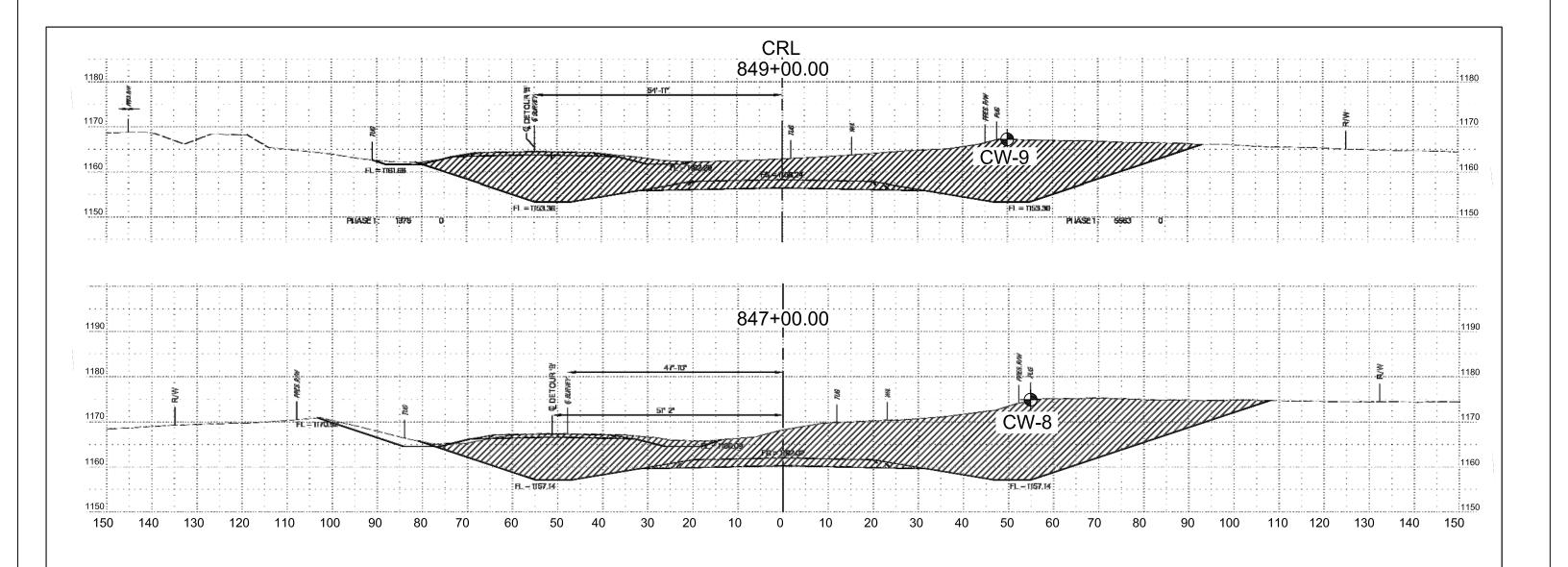
BORING LOCATIONS AND ELEVATIONS							
Boring	Elevation						
CW-5	770+00	50' Left	1141'				
CW-6	772+00	50' Left	1154.5'				
CW-7	774+00	50' Left	1142.5'				

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#### BORING LOCATION DIAGRAM - CROSS SECTIONS

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Approved By:	JWB	Sheet No.	3/4



BORING LOCATIONS AND ELEVATIONS						
Boring Station CRL Offset Elevation						
CW-8	847+00	55' right	1175'			
CW-9	849+00	50' right	1167'			

### RED ROCK CONSULTING

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#### BORING LOCATION DIAGRAM - CROSS SECTIONS

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Checked By:	JWB	Date: 8/	/17/2018
Approved By:	JWB	Sheet No.	4/4

## RED ROCK BORING NUMBER CW-1 PAGE 1 OF 1

CONSULTING

DURING AFTER CAVE IN 18043 LOGS.GPJ DATA TEMPLATE.GDT

PROJECT NAME SH 29 Cut Analysis - West Phase 1 **CLIENT** SRB PROJECT NUMBER 18043 PROJECT LOCATION Stephens County, Oklahoma DATE STARTED 5/16/18 COMPLETED 5/16/18 GROUND ELEVATION 1228 ft STATION 654+00 OFFSET 50' LT **DRILLING CONTRACTOR** DSO - Drilling Services of Oklahoma **GROUND WATER LEVELS:** DRILLING METHOD 4.5" augers - CME 750 ATV DURING DRILLING none LOGGED BY SAH **CHECKED BY** JWB 0 hrs AFTER DRILLING none NOTES JP# 29657(10) Cave In Depth none **ATTERBERG** BLOW COUNTS N SAMPLE TYPE MOISTURE CONTENT (%) ELEVATION (ft) PASSING #200 SIEVE (%) LIMITS GRAPHIC LOG DEPTH (ft) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION 0 SANDY LEAN CLAY, reddish brown with white, soft 122<del>/8'</del> SPT 24 9 64 2 15 50/6" 1227.5' **SANDSTONE**, light gray with purple, very poorly cemented to very well TC 50/4.3 1225 50/2.8" 5 50/4.3" 50/2.5" TC 1220 10 32/6" 50/4.8" TC 1215 15 50/0.8" 50/0.5" TC 1210 20 50/0.6" 50/0.3" TC 1205 25 TC 50/0.8" 50/0.3" 1200 30 50/0.6" 50/0.4" Boring Termination Depth = 31 feet 1197' TC \_ 1195 Boring Completed and Backfilled on 5/16/18 1185 1180

## BORING NUMBER CW-2 PAGE 1 OF 1

L				L	RO		I	
C	0	N	S	U	LT	1	N	G

CLI	ENT	SRB			PROJECT NA	ME SH 29 C	ut Analysi	s - Wes	t Phase	1			
PRO	OJEC.	T NUN	<b>IBER</b> 18043	3	PROJECT LO	PROJECT LOCATION Stephens County, Oklahoma							
DAT	TE ST	ARTE	<b>D</b> 5/16/18	<b>COMPLETED</b> 5/16/18	GROUND EL	GROUND ELEVATION 1226 ft STATION 656+00 OFFSET 50' LT							
DRI	LLIN	G CON	ITRACTOR _	DSO - Drilling Services of Oklahoma		ATER LEVELS							
DRI	LLIN	G MET	'HOD 4.5" a	ugers - CME 750 ATV	DURIN	G DRILLING _	none						
LO	GGED	BY _	SAH	CHECKED BY JWB	0 hrs A	FTER DRILLIN	NG none						
NO	TES _	JP# 2	9657(10)			n Depth none							
							T	m		AT	TERBI	ERG	
ELEVATION (ft)	(£)	ୁ					SAMPLE TYPE	COUNTS	MOISTURE CONTENT (%)		LIMIT	<u>S</u>	PASSING #200 SIEVE (%)
410	DEРТН (ft)	GRAPHIC LOG		MATERIAL DESCRI	PTION		<u> </u>	8z	STU EN	≙⊨	PLASTIC LIMIT	PLASTICITY INDEX	ING VE (
EV.	DEF	S. J.					MP.	BLOW	ON C	LIQUID	LAS	ASTICI INDEX	ASS SIE
	0						8	В	_ o		Ф	PL/	Δ
1225				<b>LEAN CLAY WITH SAND</b> , reddis	sh brown, medium stiff	1226'	SPT	5	21	47	19	28	72.6
	+ -												
	‡ :												
1220	5 -			SANDY LEAN CLAY, lig	ht brown hard	1221'	// apr	10	_	05	40		04.0
1229		<i>/////</i>		SANDSTONE, light gray, very poorly of			SPT	27	5	25	12	13	61.8
	∔ -	<b>∤</b> ∷∷:					<b>V</b>	50/5.5" 50/3.5"					
	10							50/4.5"					
1215	5						ТС	50/0.8" 50/0.5"					
	+ -	<del> </del> ::::							1				
:	Į:	]::::											
1210	15 <sub>_</sub>	 					ТС	50/0.8" 50/0.5"					
	1						VIC	50/0.5"	1				
	+ -	<b>∤</b> ∷∷:											
	20							50/0.00					
1205	-	-					TC	50/0.6" 50/0.4"					
	‡ :												
	25	::::  ::::											
1200				Boring Termination De		1201'	Тс	50/0.8" 50/0.4"					
	-			Boring Completed and Back	dilled on 5/16/18			50/0.4	1				
8													
/9/6 1195													
195													
<u> </u>	-												
EMP	1												
1190	0												
2 -	1												
9SS.G													
1185	5												
1804													
<u>≅</u>	1												
S CA	1												
1180	<u>)</u>												
NG -	1												
1 DURING AFTER CAVE IN 18043 LOGS.GPJ DATA TEMPLATE.GDT 9/6/18	-												
,			1										

## BORING NUMBER CW-3 PAGE 1 OF 1

K	ZI			I	20	0		I	
C	0	N	S	U	L	Т	I	N	G

1 DURING AFTER CAVE IN 18043 LOGS.GPJ DATA TEMPLATE.GDT 9/6/18

CLIE	NT _	SRB						PROJECT	NAME _	SH 29 Cı	ut Analy	sis - Wes	t Phase	: 1			
PRO	JECT	T NUM	BER _1804	3				PROJECT	LOCATIO	ON Step	hens C	ounty, Ol	klahoma	1			
			<b>D</b> 5/16/18		<del>-</del>	<b>ED</b> <u>5/16/18</u>		GROUND E	ELEVATION	ON <u>121</u>	4 ft	STATIO	N <u>676</u> -	+00 C	FFSE	<b>r</b> <u>50'</u>	LT
					illing Services	of Oklahoma	<u> </u>	GROUND V									
				augers - Cl	ME 750 ATV				ING DRIL								
		BY _			_ CHECKED	BY JWB			AFTER			e					
NOI		JF# <u>Z</u>	9657(10)					Cave	In Dept	n <u>none</u>		T	1		TEDDI	-00	
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG			MATEI	RIAL DESCF	RIPTION				SAMPLE TYPE	BLOW COUNTS N	MOISTURE CONTENT (%)	LIQUID	PLASTIC IT		PASSING #200 SIEVE (%)
ᆸ	0										/%	B	-0		П	7	Α/
					CLAYEY SA	ND, reddish	brown, very	loose		1214'	SP	Т 3	13	32	12	20	48.4
 121 <u>0</u>	   5 _																
				LE	AN CLAY WIT	TH SAND, re	ddish brown	ı, very stiff		1209'	SP	T 25	10	43	15	28	81.1
 1205 																	
		<del>                                   </del>		SANDSTO	SANDY SIL DNE, light gray	<u>T</u> , reddish br			, well	120 <del>4'</del> 1203.5'	SP TO	¬ 50/6"	7	0	0	NP	53.9
1200  - 1195  1190						cemente				4400	тс	50/0.5	-				
1185 1180 1175 11770 11765 1165					Boring Compl	ermination Di				1189'	TO	50/0.5					

## BORING NUMBER CW-4 PAGE 1 OF 1

R				I	20	0		I	
C	0	N	S	U	L	T	1	N	G

1 DURING AFTER CAVE IN 18043 LOGS.GPJ DATA TEMPLATE.GDT 9/6/18

CLIE	ENT	SRB		PROJECT NAME SH	H 29 Cu	ıt Analysis	s - West	: Phase	1			
	_		BER 18043	PROJECT LOCATION								
DAT	E ST	ARTE	<b>D</b> <u>7/13/18</u> <b>COMPLETED</b> <u>7/13/18</u>	_ GROUND ELEVATION	<b>N</b> 119	1.5 ft <b>S</b>	TATION	682+	- <u>59</u> <b>o</b>	FFSE	<b>r</b> 95'	LT
DRII	LING	CON	TRACTOR DSO - Drilling Services of Oklahoma									
DRII	LINC	MET	HOD _4.5" augers - CME 750 ATV	$_{\perp}$ $\stackrel{ extstyle  op}{=}$ during drill								
LOG	GED	BY _	SAH CHECKED BY JWB	_ To hrs AFTER D		<b>G</b> 21.0 f	t / Elev	1170.5	ft			
NOT	ES _	JP# 2	9657(10)	_ Cave In Depth	none							
Œ						Щ	TS	(%		TERBE LIMITS		00
O	DEРТН (ft)	GRAPHIC LOG				Σ	NNC	URE (S)				3 #2
ΑTI	∃PT⊦	RA P I	MATERIAL DESCRIPTION			PLE	N CC	JST TEP	LIQUID	STIC	들찄	SINC
ELEVATION (ft)	DE	Ō				SAMPLE TYPE	BLOW COUNTS N	MOISTURE CONTENT (%)		PLASTIC LIMIT	PLASTICITY INDEX	PASSING #200 SIEVE (%)
	0	/////	SANDY LEAN CLAY, orangish brow	wn etiff 1	191.5'	V						
			SANDI ELAN CLAT, Clangish blow	wii, Suii i	191.5	SPT	14	8	27	13	14	50.5
	-											
	5 _											
_ 1185	-		<u>SILTY SAND</u> , orangish brown, mediu	m dense 1	186.5'	SPT	17	7	0	0	NP	42.5
	-											
	- 10											
1180						SPT	16	4	0	0	NP	30.0
	<u> </u>											
	15											
_ 117 <u>5</u>	-		SILTY, CLAYEY SAND, light gray, med	lium dense 1	176.5'	SPT	22	4	23	17	6	28.6
	-				ĺ							
	_20_	/ <u>//!!</u>	▼ SANDSTONE, orangish brown, well cemented to	very well cemented 1	171.5'	≤ SPT,	50/5.8")	10	21	15	6	40.5
1170			<del></del>	•		TC	50/1" 50/0.4"/					
			$\bar{\Delta}$									
	_25_	::::										
<u>1</u> 165			Boring Termination Depth = 25.5 Boring Completed and Grouted on 7	feet 7/13/18	1166'	TC	50/0.3" 50/0.1" <sub>/</sub>					
1160												
_ 1155												
_ 												
1150												

## RED ROCK CONSULTING BORING NUMBER CW-5 PAGE 1 OF 1

PROJECT NAME SH 29 Cut Analysis - West Phase 1

PROJECT NUMBER 18043

PROJECT LOCATION Stephens County, Oklahoma

DATE STARTED 7/11/18 COMPLETED 7/11/18

DRILLING CONTRACTOR DSO - Drilling Services of Oklahoma

DRILLING METHOD 4.5" augers - CME 750 ATV

LOGGED BY SAH CHECKED BY JWB PROJECT NAME SH 29 Cut Analysis - West Phase 1

PROJECT NAME SH 29 Cut Analysis - West Phase 1

PROJECT NAME SH 29 Cut Analysis - West Phase 1

PROJECT NAME SH 29 Cut Analysis - West Phase 1

GROUND ELEVATION 1141 ft STATION 770+00 OFFSET 50' LT

DRILLING CONTRACTOR DSO - Drilling Services of Oklahoma

DRILLING METHOD 4.5" augers - CME 750 ATV

LOGGED BY SAH CHECKED BY JWB Phase 1

Cave in Depth none

DRILLIN	G METHOD 4.5" a	augers - CME 750 ATV	UPTION  DURING DRILLING 15.0 ft / Elev 1126.0 ft  ▼ 0 hrs AFTER DRILLING 16.5 ft / Elev 1124.5 ft  Cave In Depth none  Student Studen									
	DBY SAH	CHECKED BY JWB			<b>G</b> 16.5 f	t / Elev	1124.5	ft				
NOTES	JP# 29657(10)		Cave In Depth	none								
ELEVATION (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION			SAMPLE TYPE	BLOW COUNTS N	MOISTURE CONTENT (%)	LIQUID	LIMIT	PLASTICITY SINDEX	PASSING #200 SIEVE (%)	
1140		SILTY SAND, brown, loose		1141'	SPT	8	4	0	0	NP	22.0	
1135 10 1130 15 1125 20 1120 25 1115	\( \sqrt{1}\)	SANDY SILTY CLAY, reddish brown, ver SANDSTONE, light gray, poorly cemented to we		1136' 1135'	TC TC	13 30 50/5" 50/1.8" 50/1.8" 50/1.8" 50/0.4" 50/0.4" 50/0.5"	8	22	15	7	55.	
30 1110 		Boring Termination Depth = 30 feet Boring Completed and Grouted on 7/11	t 1/18	1111'	ТС	50/0.8" 50/0.4"						

### BORING NUMBER CW-6 PAGE 1 OF 1 RED ROCK CONSULTING

	_	SRB T NUN	BER 18043	<pre>PROJECT NAME SH PROJECT LOCATION</pre>								
DAT	E ST	ARTE	D _7/12/18	_ GROUND ELEVATION	1 115	4.5 ft <b>S</b>				FFSE	<b>T</b> 50'	LT
			TRACTOR DSO - Drilling Services of Oklahoma  HOD wet rotary - CME 750 ATV	_ GROUND WATER LE\ _ DURING DRILLI								
			SAH CHECKED BY JWB	_ 0 hrs AFTER DF								
		_	9657(10)	Cave In Depth _								
Œ.						Й	TS	©	АТ	TERB LIMIT		8
ELEVATION (ft)	O DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION			SAMPLE TYPE	BLOW COUNTS N	MOISTURE CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	PASSING #200 SIEVE (%)
	-		SILTY, CLAYEY SAND, light brown, me	edium dense 11	54.5'	SPT	20	5	23	16	7	30.4
	-  -  -											
_ 1150	5 _		<u>SILTY SAND</u> , light brown, very d		50, <del>5'</del>		30	8	0	0	NP	23.0
 	 		<b>SANDSTONE</b> , light gray, poorly cemented to v	ery well cemented	1150'	TC TC	50/4" 50/3" 50/2"					
114 <u>5</u>	_ _10_						50/1 Q"					
 	-  -  -					TC	50/1.8" 50/1"					
<u>1</u> 14 <u>0</u>	15_						E0/0.2"					
 	 					TC	50/0.3" 50/0.3"					
_ 113 <u>5</u>	20						E0/0 4"					
 	-  -  -					TC	50/0.4" 50/0.3"					
_ 113 <u>0</u> _	25_						50/0 5"					
 	 					▼ IC	50/0.5" 50/0.3"					
_ 112 <u>5</u> 	_ _30_					▼ TC	50/0.4" 50/0.1"					
 	- 						50/0.1					
112 <u>0</u> 	_35_ 					ТС	50/1" 50/0.4"					
 _ <u>1</u> 115	  											
 	_40_ 					TC	50/0.8" 50/0.4"					
 	45											
 	- **- 		Boring Termination Depth = 45 Boring Completed and Backfilled on	feet 11 7/12/18	09.5'	TC	50/0.8" 50/0.5"					
 _ _110 <u>5</u>												

## BORING NUMBER CW-7 PAGE 1 OF 1

I	ZI			I	P	0		I	
C	0	N	S	U	L	T	I	N	G

CLI	ENT .	SRB		_ PROJECT NAME	SH 29 C	ut Analysi	s - Wes	t Phase	1			
PRO	JEC.	T NUN	MBER 18043	_ PROJECT LOCAT	ION Step	hens Cou	ınty, Ok	lahoma	l			
DAT	TE ST	ARTE	ED _7/11/18	_ GROUND ELEVAT	ION _114	2.5 ft <b>S</b>	TATION	774	<u>+00</u> <b>c</b>	FFSE	T 50'	LT
DRI	LLING	G CON	NTRACTOR DSO - Drilling Services of Oklahoma	_ GROUND WATER	LEVELS:							
DRI	LLING	S MET	THOD 4.5" augers - CME 750 ATV	DURING DR	ILLING _	none						
LOC	GED	BY _	SAH CHECKED BY JWB	_ 0 hrs AFTEF	R DRILLIN	IG none						
NOT	res _	JP# 2	9657(10)	_ Cave In Dep	oth none							
Ð						111	ဟ		AT	TERB		0
Z) (H)	Œ	ပ္				SAMPLE TYPE	COUNTS	MOISTURE CONTENT (%)		LIMIT		PASSING #200 SIEVE (%)
ELEVATION	DEРТН (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION			<u> </u>	Öz	STU EN	₽⊨	일	PLASTICITY INDEX	NG VE (
	DEF	유 _				₩	BLOW	<u>S</u> N	LIQUID	PLASTIC LIMIT	ASTIC	SS
=	0					/\$	В	_ o			7	Δ
			SANDY LEAN CLAY, reddish brov	vn, stiff	1142.5'	SPT	11	11	25	16	9	51.3
1140	<u> </u>											
	_ 5 _	/////	SANDSTONE, light gray with reddish brown, ce	omented to very well	1127 5'	SPT	50/5"	4	. 0	. 0	NP /	24.1
			cemented	erilerited to very well	1137.3	TC	50/1.3"	<u> </u>				27.1
1135	P -						50/0.8	1				
	10											
-						TC	50/1.3" 50/0.5"					
1130	j						,50/0.5	1				
	_15_	::::					50/1"					
1105						TC	50/0.3"					
1125	<u> </u> 											
	20											
	[					TC	50/1.5" 50/1"					
1120	j						00/1	1				
	_25_	::::				TC TC	50/1"					
1115	-					TC	50/1" 50/0.4"					
	} -											
9/6/18	30											
5			Boring Termination Depth = 30 Boring Completed and Backfilled on	feet 7/11/18	1112.5'	TC	50/0.4" 50/0.4"					
1110	)		Borning Completed and Basianisa on	7,71,710				]				
MPL/												
A TE												
<b>A</b>												
GPJ												
890												
30431												
<sup>∞</sup> 1100	)											
AVE -												
- ER C												
1095	5											
1 DURING AFTER CAVE IN 18043 LOGS.GPJ DATA TEMPLATE.GDT 9/6/18	1											
<u> </u>	-											

## BORING NUMBER CW-8 PAGE 1 OF 1

I				I	R		CI	
C	0	N	S	U	L	ΤI	N	G

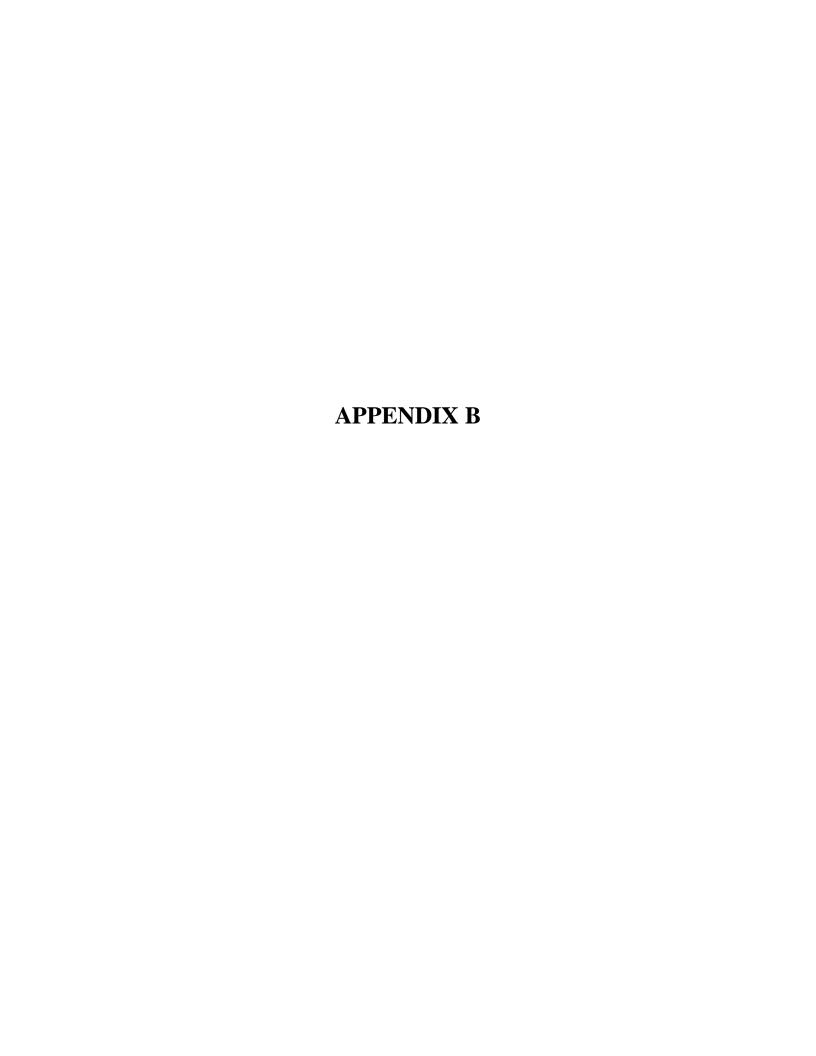
1 DURING AFTER CAVE IN 18043 LOGS.GPJ DATA TEMPLATE.GDT 9/6/18

PROJECT NAME SH 25  PROJECT NUMBER 18043 PROJECT LOCATION S  DATE STARTED 5/16/18 COMPLETED 5/16/18 GROUND ELEVATION DRILLING CONTRACTOR DSO - Drilling Services of Oklahoma GROUND WATER LEVE	175 ft  S: 10.0 ft /	ounty, Ol	klahoma	1	DEESE	<b>T</b> 551	
DATE STARTED     5/16/18     COMPLETED     5/16/18     GROUND ELEVATION       DRILLING CONTRACTOR     DSO - Drilling Services of Oklahoma     GROUND WATER LEVE	_S: 10.0 ft / LING12.		N 847	+00 (	)FFSF	<b>-</b>	
		Elev 116			<i>)</i> , , or	1 <u>55</u>	RT
DDILLING METHOD 4 FILEWARD CASE 750 ATV	LING 12.	Elev 116					
DRILLING METHOD <u>4.5" augers - CME 750 ATV</u> $\underline{\underline{\nabla}}$ DURING DRILLING							
LOGGED BY SAH CHECKED BY JWB ▼0 hrs AFTER DRIL		0 ft / Elev	1163.0	ft			
NOTES _JP# 29657(10)	ne						
(£)	Ш	ST3	(%	Α٦	ITERB LIMIT		000
MATERIAL DESCRIPTION  (t)  (C)  (C)  (C)  (C)  (C)  (C)  (C)	SAMPLE TYPE	BLOW COUNTS N	MOISTURE CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	PASSING #200 SIEVE (%)
1175 0   SILTY SAND, reddish brown, medium dense 117	'5' SF		9	0	0	NP	32.6
	<u> </u>						
170 5 SANDSTONE, reddish brown with interbedded light gray layers, cemented to well cemented	SF TO	T, 50/4" 50/1.3' 50/0.8'	5	0_	<u> </u>	NP_	
	T	50/1.3'	<u> </u>   				
_	Т	50/0.8'	<u> </u>				
115 <u>5</u> 20	Т	50/1" 50/0.5					
1150 25	TO	50/0.8'	<u>-</u>				
Boring Termination Depth = 29.5 feet 1145 Boring Completed and Grouted on 5/16/18	5' T	50/0.8' 50/0.6'					
  113 <u>5</u>							
   1130							
113 <u>0</u> 							

## BORING NUMBER CW-9 PAGE 1 OF 1

K	ZI			L	R	0		I	
C	0	N	S	U	L	T	I	N	G

CLII	ENT	SRB			PROJECT NAME	SH 29 C	ut Analysis	s - West	t Phase	1			
PRO	)JEC	NUM	IBER <u>18043</u>		_ PROJECT LOCAT	ION Ste	phens Cou	ınty, Ok	lahoma				
DAT	E ST	ARTE	<b>D</b> 5/16/18	COMPLETED _5/16/18	_ GROUND ELEVAT	TION _116	67 ft <b>S</b>	TATION	<b>1</b> 849+	<u>-00</u> C	FFSE	<b>T</b> _50'	RT
				SO - Drilling Services of Oklahoma	_ GROUND WATER	LEVELS	:						
DRI	LLING	MET	<b>HOD</b> 4.5" auge	ers - CME 750 ATV	_ DURING DR	ILLING _	none						
LOC	GED	BY _	SAH	CHECKED BY JWB	_ 0 hrs AFTE	R DRILLIN	IG none						
NOT	res _	JP# 2	9657(10)		_ Cave In Dep	oth none							
Œ							ш	S	(9)	AT	TERB LIMIT		00
ELEVATION (ft)	€	GRAPHIC LOG					SAMPLE TYPE	COUNTS	MOISTURE CONTENT (%)				PASSING #200 SIEVE (%)
ATIC	DEРТН (ft)	Name		MATERIAL DESCRIPTION			<u>ا</u> ا	8z	IST	음투	F	듣쬬	N N N
le l	DE	<u>β</u>					AME	BLOW	δÑ	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	ASS
Ш	0						S	B			ш	П	Δ.
1165	-			<b>LEAN CLAY WITH SAND</b> , reddish brown,	light gray, stiff	1167'	SPT	12	8	24	16	8	78.9
1105	<u> </u>												
-	ļ <sub>-</sub> -			CANDETONE reddish brown light grov conserve	antad to vanculal	1162	≥ SPT	50/3"	4	v 33 /	17	v 16 /	52.2
	_ 5 _		<u> </u>	<b>SANDSTONE</b> , reddish brown, light gray, cem cemented	ented to very well	1163	TC	50/1"		\_33_/		16/	32.2
1160		:::::						50/0.5"	1				
	-												
	10						TC	50/0.8"	_				
_ 1155	-						V IC	50/0.5"	1				
	_ 												
	<u> </u>						TC	50/0.5" 50/0.3"					
1150	-	::::											
	_												
	20						TC TC	50/1.3"					
1145	-  -						<b>▼</b> 1.5	50/1"	1				
	-	:::: <u>:</u>						50/4"					
				Boring Termination Depth = 24.5 Boring Completed and Backfilled on		1142.5'	TC	50/1" 50/0.4"					
1140	<u>)</u>												
8													
/9/6 _													
[] 1135	5												
-   													
HE													
¥ 1130													
<u> </u>	4												
GS:G													
9													
₫ 1125													
필													
A CA													
巴 上 1120													
1 1 1 2 C													
1 DURING AFTER CAVE IN 18043 LOGS.GPJ DATA TEMPLATE.GDT 9/6/18													



#### **SUMMARY OF LABORATORY RESULTS**



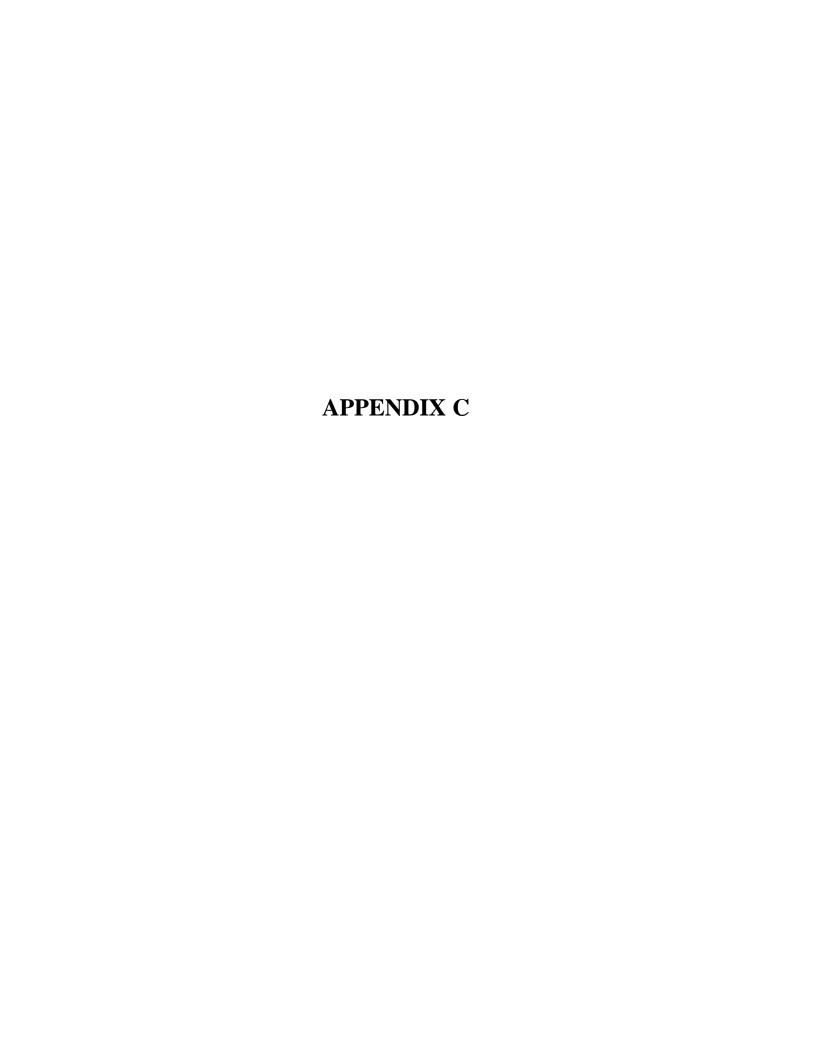
P.O. Box 30591 73003

Telephone: 405-562-3328

PROJECT NUMBER18043PROJECT NAMESH 29 Cut Analysis - West Phase 1

CLIENT SRB

Borehole	Depth (ft)	% Moist.	Liquid Limit	Plastic Limit	Plastic Index	-3" Sieve	-3/4" Sieve	-1/2" Sieve	-4 Sieve	-10 Sieve	-40 Sieve	-200 Sieve	рН	Resistivity (Ω-cm)	Sulfates (ppm)
CW-1	0	2.2	24	15	9	100	100	100	99	96	82	64.0			
CW-2	0	20.6	47	19	28	100	100	100	100	100	100	72.6			
CW-2	5	5.1	25	12	13	100	100	100	100	99	97	61.8			
CW-3	0	13.2	32	12	20	100	100	100	100	100	100	48.4			
CW-3	5	9.6	43	15	28	100	100	100	100	100	99	81.1			
CW-3	10	6.6	NV	NP	NP	100	100	100	100	100	100	53.9			
CW-4	0	8.2	27	13	14	100	100	100	100	100	100	50.5			
CW-4	5	6.6	NV	NP	NP	100	100	100	100	100	100	42.5			
CW-4	10	3.5	NV	NP	NP	100	100	100	100	100	100	30.0			
CW-4	15	4.3	23	17	6	100	100	100	98	97	95	28.6			
CW-4	20	10.4	21	15	6	100	100	100	100	100	99	40.5			
CW-5	0	4.4	NV	NP	NP	100	100	100	100	100	96	22.6			
CW-5	5	7.5	22	15	7	100	100	100	99	98	96	55.8			
CW-6	0	4.6	23	16	7	100	100	100	100	100	99	30.4			
CW-6	4	8.2	NV	NP	NP	100	100	100	100	100	98	23.0			
CW-7	0	11.1	25	16	9	100	100	100	100	100	99	51.3			
CW-7	5	4.2	NV	NP	NP	100	100	100	100	100	99	24.1			
CW-8	0	8.8	NV	NP	NP	100	100	100	100	100	98	32.6			
CW-8	4	4.6	NV	NP	NP	100	100	100	99	97	80	29.6			
CW-9	0	7.8	24	16	8	100	100	100	99	98	97	78.9			
CW-9	4	3.7	33	17	16	100	100	100	100	100	99	52.2			





#### **GENERAL NOTES**

#### SOIL PROPERTY ABBREVIATIONS

 $\begin{array}{ll} N & & \text{Uncorrected SPT Penetration, blows per foot} \\ N_{60} & & \text{Corrected SPT Penetration, blows per foot} \\ Q_u & & \text{Unconfined Compressive Strength, psf} \\ Mc & & \text{Moisture Content, \%} \end{array}$ 

LL Liquid Limit, %
PL Plastic Limit, %
PI Plasticity Index, %

#### **DRILLING & SAMPLING ABBREVIATIONS**

BS Bag Sample
SPT Split Spoon Sample
ST Shelby Tube Sample

AU Auger Sample
TC Texas Cone Penetrometer

DCP Dynamic Cone Penetrometer

## UNIFIED SOIL CLASSIFICATION SYSTEM (ASTM D 2487) -- used to classify all soils unless otherwise noted --

Major Divisions			Group	
			Symbol	Typical Names
Course-Grained Soils	Gravels		GW	Well-graded gravels and gravel-sand mixtures, little or no fines
>50% retained on #200 sieve	50% + of course fraction retained on	Clean Gravels	GP	Poorly graded gravels and gravel-sand mixtures, little or no fines
	#4 sieve	Gravels	GM	Silty gravels, gravel-sand-silt mixtures
		with Fines	GC	Clayey gravels, gravel-sand-clay mixtures
	Sands		SW	Well-graded sands and gravelly sands, little or no fines
	50% + of course fraction passes #4	Clean Sands	SP	Poorly graded sands and gravelly sands, little or no fines
	sieve	Sands	SM	Silty sands, sand-silt mixtures
		with Fines	SC	Clayey sands, sand-clay mixtures
Fine-Grained Soils	Silts and Clays		ML	Inorganic silts, very fine sands, rock four, silty or clayey fine sands
<50% passes #200 sieve	Liquid Limit ≤ 50%		CL	Inorganic clays of low to medium plasticity, gravelly/sandy/silty/lean clays
			OL	Organic silts and organic silty clays of low plasticity
	Silts and Clays		МН	Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts
	Liquid Limit > 50%		СН	Inorganic clays or high plasticity, fat clays
			ОН	Organic clays of medium to high plasticity
Highly Organic Soils			PT	Peat, muck, and other highly organic soils

Prefix: G = Gravel, S = Sand, M = Silt, C = Clay, O = Organic

Suffix: W = Well Graded, P = Poorly Graded, M = Silty, L = Clay, LL < 50%, H = Clay, LL > 50%

#### PLASTICITY OF COHESIVE SOIL

1 = 10 110 11 01 00 11 = 011 = 011			
Degree of Plasticity	Plasticity Index	Swell Potential	
None	0 to 4	Very Low	
Slight	5 to 9	Low	
Medium	10 to 19	Low to Medium	
High	20 to 39	Medium to High	
Very High	40+	Very High	

#### MOISTURE OF COHESIVE SOIL

Description	Condition	Moisture Content
Dry, Dusty	Dry	0 to 10%
Damp	Moist	10 to 30%
Free Water	Wet	30 to 70%

#### **CONSISTENCY - COHESIVE SOILS**

Consistency	SPT
Very Soft	<2
Soft	2 to 4
Medium Stiff	5 to 8
Stiff	9 to 14
Very Stiff	15 to 30
Hard	31+

#### **DENSITY - COHESIONLESS SOILS**

Relative Density	SPT
Very Loose	<4
Loose	4 to 10
Medium Dense	11 to 30
Dense	31 to 50
Very Dense	51+

#### **ROCK HARDNESS**

SPT (in/50)	TCP (in/100)	Rock Description
6+	6+	Very Soft / Very Poorly Cemented
5 - 6	3 - 6	Soft / Poorly Cemented
4 - 5	2 - 3	Moderately Hard / Cemented
3 - 4	1 - 2	Hard / Well Cemented
<3	<1	Very Hard / Very Well Cemented

#### **ROCK CORE QUALITY**

Core Quality	RQD
Excellent Quality	90 – 100%
Good Quality	75 – 90%
Fair Quality	50 – 75%
Poor Quality	25 – 50%
Very Poor Quality	<25%