Fracture Critical Bridge Inspection Report

NBI Bridge No.: 17611

Route S.H. 100 over ARKANSAS RIVER
Muskogee County



Prepared for:

Oklahoma Department of Transportation Field District 01

Inspection Date:

7/14/2023



Report Prepared By:

BURGESS & NIPLE, INC.

141 N.E. 13th St. Suite 114A Oklahoma City, OK 73104 405-759-4141 **BURGESS & NIPLE** Engineers • Surveyors • Planners

BURGESS & NIPLE

2100 N Eastern Ave, Suite 8B | Moore, OK 73160 | 405.434.6525

Mr. Wes Kellogg, P.E. Field Service Engineer Oklahoma Department of

Transportation

200 Northeast 21st Street Oklahoma City, OK 73102-3204 Re: Fracture Critical Bridge Inspection Report

Structure No.: 5159 0300X

NBI No.: 17611

S.H. 100 over Arkansas River

Muskogee County
ODOT Field Division 1

August 11, 2023

Dear Mr. Kellogg:

Burgess & Niple (B&N) performed a fracture critical and routine inspection of the above referenced bridge on July 13 and 14, 2023. The bridge is a fifteen-span structure (photos 1 and 2) with spans numbered from west to east and consisting of:

Spans 1 - 4: Four 100-foot-long continuous steel multi girders spans

Spans 5 - 7: Three span continuous steel twin girders (207 feet - 334 feet - 207 feet)

Spans 8 - 10: Three 100-foot-long continuous steel multi girders spans Spans 11 - 14: Four 100-foot-long continuous steel multi girders spans

Span 15: One 100-foot-long simple steel multi girder span

The limits of the inspection were from the west abutment to the east abutment. Inspection team members included Shaun Fillmore, PE (Team Leader), Dale Poorman, PE, Jarrett Shafer, EI, Drew Urban, EI, and Patrick Kalush.

As per the latest load rating report date November 24, 2003, the bridge does not require a load posting. This bridge was recently rehabilitated in 2014; see the 17611(2014-05-29)FC report for further details regarding the rehabilitation.

This report includes appendices containing:

- Significant Findings
- Truss/FC Bridge Rating Form
- Condition Photographs
- Oklahoma DOT Bridge Inspection Form/BrM element report



The current and previous NBI ratings for the bridge are:

NBI Item	Current Rating (2021)	Previous Rating (2019)
NBI Item 58 (Deck)	6 = Satisfactory	6 = Satisfactory
NBI Item 59 (Superstructure)	5 = Fair	5 = Fair
NBI Item 60 (Substructure)	6 = Satisfactory	6 = Satisfactory
NBI Item 61 (Channel)	6 = Bank Slumping	6 = Bank Slumping
NBI Item 113 (Scour)	(8 = Calculated Scour Above	(8 = Calculated Scour Above
	Foundation)	Foundation)
Sufficiency Rating	66.7 (ND)	66.7 (ND)

The bridge is neither structurally deficient nor functionally obsolete.

RECOMMENDED ACTIONS, in order of decreasing priority, are as follows:

Priority Code **CX** – Bridge condition is bad enough that there is a possibility of failure of a major structural component if repairs are not completed within the next few days.

No CX repair items are required at this time.

Priority Code **PX** – Bridge condition is such that immediate repair is not necessary but should be completed within the next several weeks or months.

- Replace north railing post anchor bolts missing from the eastern most railing post.
- Unclog the deck scuppers.
- Reseal the fixed poured joint seal at both abutments.
- Arrest girder web cracks at the horizontal splice termination at:
 - Span 5, girder 1 at the field splice near floor beam 5 5/8-inch-long crack with no arrestor hole.
 - Span 6, girder 2 near floor beam 11 3/16-inch-long vertical crack in the lower web plate.
- Replace missing bolts and tighten loose bolts at
 - Girder splice locations
 - Floor beam connection to the girders in spans 5, 6 and 7.
 - Stringer connection to floor beams in spans 5, 6 and 7.
- Repair cracked web connection plate weld for floor beam 6 in span 5 at girder 1.
- Reattach floor beam 0 lower connection to girder 2 in span 6. Consider bolting the previously welded connection.
- Repair cracks in the lower lateral bracing in span 5, floor beam 7, girder 2 and span 6, floor beam 12, girder 2.
- Tighten loose anchor bolts and replace missing or bent anchor bolts.

Priority Code **FX** – Bridge condition is such that repair should not be necessary any time soon, monitor during future inspections.

- Monitor the deck soffit along the girders, floor beams and stringers for further spalls falling into the channel.
- Monitor the vertical offset of the finger joints for changes in height at piers 4 and 7.
- Monitor locations of girder web cracks having drilled hole retrofits or paint cracks at the horizontal splice termination at:
 - Span 5, girder 2 at the field splice near floor beam 5 paint crack.
 - Span 6, girder 1 at the field splice near floor beam 3 arrested crack.
 - Span 7, girder 1 at the field splice near floor beam 4 paint crack.
 - Span 7, girder 2 at the field splice near floor beam 4 arrested crack.
- Monitor the 1 1/4-inch long paint crack in the span 5, girder 1 web at the longitudinal stiffener cored hole between floor beams 4 and 5 (perform Magnetic Particle Testing during 2022 Other/Special inspection).
- Monitor cored hole locations in the longitudinal stiffeners for crack development in the girder web.
- Monitor bow in the web of girder 1, span 7 at the field splice between floor beams 3 and 4.
- Monitor cracked welds at cross frame connection to girders due to pack rust.
- Monitor cracks at the stringer connection angles at:
 - o Span 5, stringer 3 connection to floor beam 3
 - Span 7, stringer 1 connection to floor beam 0
 - Span 7, stringer 3 connection to floor beam 0
- Monitor welded connections at recently replaced floor beams due to irregular weld contour.

It is recommended that this structure remain on a 24-month Routine/Fracture Critical inspection frequency and a 24-month Other/Special inspection frequency.

Other/Special Inspection items include:

- Girder web cracks at:
 - Span 5, girder 1 (south face) between floor beams 4 and 5 1 1/4-inch-long paint crack in web at the longitudinal stiffener cored hole (perform Magnetic Particle Testing during 2022 Other/Special inspection)
 - Span 5, girder 1 at the field splice near floor beam 5 5/8-inch-long crack with no arrestor hole.
 - Span 5, girder 2 at the field splice near floor beam 5 paint crack.
 - o Span 6, girder 1 at the field splice near floor beam 3 arrested crack.
 - Span 6, girder 2 near floor beam 11 3/16-inch-long crack.
 - Span 7, girder 1 at the field splice near floor beam 4 paint crack.
 - Span 7, girder 2 at the field splice near floor beam 4 arrested crack.
- Cracks in the stringer connection angles welds to replaced floor beams at:
 - Span 5, stringer 3 connection to floor beam 3
 - Span 7, stringer 1 connection to floor beam 0
 - Span 7, stringer 3 connection to floor beam 0
- Crack on exterior face of span 15, beam 1 in near pier 14.

- Cracked floor beam to girder connection welds:
 - Span 5, floor beam 6 upper connection to girder 1 − 5 1/8-inch-long crack in connection plate weld.
 - Span 6, floor beam 0 lower connection to girder 2 horizontal weld cracked full length.
 - Span 7, floor beam 0 lower connection to girder 2 − 1 1/8-inch-long and 1/2-inch-long cracks in welded repair.

We thank you for the opportunity to provide our engineering services. Please contact me if you have any questions or comments.

Sincerely,

BURGESS & NIPLE, INC.

Shaun Fillmore, PE Team Leader

Attachments

SIGNIFICANT FINDINGS are as follows:

NBI Item 36 – Traffic Safety (5 = Fair condition)

• **PX** – The easternmost rail post along the north barrier at the end of the east approach slab is missing all four anchor bolts **(photo 3)**.

- Span 5 sidewalk near piers 4 and 5 exhibits spalling. These are not significant and have not changed since the prior inspection.
- East sidewalk in span 3 exhibits a 15-square-foot delamination.
- Corrosion holes through the steel tube were observed through the south bridge rail near floor beam 7, span 7, and in the north bridge railing in span 6, near pier 6 (photo 4).
- The west termination of the north bridge railing is missing one rail post.
- The northeast approach railing exhibits multiple twisted/damaged blockouts (photo 5). The southeast approach railing near the east end of the bridge exhibits collision damage to the approach rail and post for 60 feet from the end of the bridge.
- The south metal rail near floor beam 3, span 10 exhibits minor impact damage.
- Isolated areas of the steel railing painted coating exhibit peeling paint due to adhesion failure between the top and intermediate coats (photo 6). Areas of corrosion are beginning to blead through. Isolated areas of the concrete rail skim coat exhibit minor cracking.
- Minor debris exists along the toe of both the north and south barriers.
- The curbs exhibit active vertical cracks and small spalls with exposed reinforcing due to insufficient cover (photo 7). These are not currently problematic.
- Tapered concrete curbs have been installed at both approaches to address blunt impact
 potential apart from the northeast corner. The northeast approach safety curb extends 14
 inches from the face of the railing and is unprotected, creating a blunt end at the transition
 (photo 8).
- All traffic safety items meet current standards for non-National Highway system roadways except for the bridge railing.

NBI Item 58 – Deck (6 = Satisfactory condition)

Driving Surface – (6 = Satisfactory condition) *The following conditions are considered minor deterioration.*

- **PX** Minor to moderate debris accumulation exists along the curbs. Several scuppers are clogged or partially clogged with vegetation (photo 9).
- The 2014 epoxy grit overlay is failing in patches throughout the deck, mostly along the wheel lines.
- Isolated shallow spalls exist in the deck, a few of which exhibit exposed and corroded reinforcing steel (photo 10).
- Transverse cracks spaced at 1 to 3 feet exist on the surface randomly along the full length of the bridge. Cracks are widest and most prominent in the twin girder spans (photo 11).
- Concrete deck patches exist throughout the driving surface from a prior rehabilitation (photo 12). Isolated spalls have been patched with asphalt (photo 13). The concrete patches are functioning as intended and the asphalt patches exhibit some deterioration.

Soffit – (6 = Satisfactory condition) *The following conditions are considered minor deterioration.*

- **FX** Isolated spalls typically 4 to 6 square feet and up to 3/4 inch deep with exposed reinforcing steel exist on the soffit **(photo 14)**. These spalls are not currently problematic.
- **FX** Shallow spalls are common along the top flange of girders, floor beams, and stringers. Isolated locations have larger spalls up to 1-foot-wide with exposed corroding reinforcing steel **(photo 15)**. This spalling is most likely due to pack rust between the superstructure and the deck.
- Isolated areas of the deck have lifted from the top flange of the girders or floor beams due to pack rust.
- Multiple 1/4-inch-wide cracks exist along the stringer deck haunch at locations in span 6 where stringers are not continuous over floor beam members.
- The deck soffit exhibits random transverse cracking with efflorescence throughout. The cracking is heaviest within 3 floor beams/diaphragms of the piers and is typically spaced at 5 feet. The cracks are due to flexure in the negative moment region over the piers. Shrinkage and hairline map cracking is common throughout.
- Bird nesting along soffit adjacent to the top flange of the girders is typical; this is heaviest in the main spans.
- Many scuppers in the main spans are sealed off with closed cell spray foam. It appears this
 foam was temporarily installed during the recent deck overlay installation and was not
 removed at all locations.

Joints – (6 = Satisfactory condition) *The following conditions are considered minor deterioration.*

- PX The poured fixed joint at the abutments exhibits minor to moderate debris impaction, debonded seals, and a few shallow spalls and patches in the headers (photo 16).
- **FX** The poured fixed joint armor at the west abutment exhibits a 1-inch vertical offset with the deck armor lower than the approach armor.
- The finger joints at piers 4 and 7 have an elastomeric trough under the joints. Debris has filled the trough causing debris impaction with most severe conditions observed at the shoulders (photo 17). The seal is torn at pier 7 (photo 18).
- Two 5-foot-long sections of the pier 4 finger joint have been replaced with a welded steel plate (photo 17). Both finger joints have a slight vertical offset of 1/8 to 3/8 inch.
- Poured seal deck control joints are typically spaced at 18 feet in the approach spans and at 50 to 75 feet in the main spans. Joint seals exhibit areas of failure and the joint headers exhibit cracking and/or spalling up to 2 feet long and 2 inches wide, some with exposed reinforcement. Isolated areas have been patched with asphalt since the previous inspection (photo 19).
- The sealed expansion joints at the west abutment, and over piers 10 and 14 have been replaced and have moderate debris impaction. Sealed expansion joints are all nearly closed.

NBI Item 59 – Superstructure (5 = Fair condition)

Fracture Critical Member Rating Summary			
Girders	5 = Fair condition		
Floor Beams	5 = Fair condition		

[FCM] Girders – (5 = Fair condition)

Fracture Critical twin girder spans exist in spans 5 through 7 and have the following comments:

- **PX/FX** Cracks were observed at the ends of the horizontal splice at the following locations. No changes were noted to the cracks unless noted otherwise.
 - **PX** Span 5, girder 1 at the field splice near floor beam 5 5/8-inch-long crack with no arrestor hole on interior face (**photo 20**).
 - FX Span 5, girder 2 at the field splice near floor beam 5 3/8-inch-long likely paint crack in the girder web at the toe of the longitudinal stiffener to web weld and has no arrestor hole (photo 21).
 - **FX** Span 6, girder 1 at the field splice near floor beam 3 3/4-inch-long crack arrested with two drilled hole retrofits **(photo 22)**. The crack has not propagated past the arrestor holes; however, two paint cracks exist in the underside of the top drilled hole.
 - PX Span 6, girder 2 near floor beam 11 3/16-inch-long vertical crack in the lower web plate without arrestor holes (photo 23). This crack was discovered during the 2020 OS inspection.
 - \circ **FX** Span 7, girder 1 near floor beam 4 1-inch-long paint crack in the upper web arrested with a arrestor hole, and 1 1/8-inch-long paint crack in the lower web that is not arrested (photo 24).
 - FX Span 7, girder 2 near floor beam 4 Two vertical cracks arrested with drilled hole retrofits (photo 25).
- PX Missing or loose bolts were observed at the following locations:
 - Span 5, girder 2, near floor beam 5.
 - Span 6, girder 1, exterior face top flange.
 - Span 6, girder 1, interior face horizontal splice over pier 6 (photo 26).
 - Span 6, girder 2, exterior face top and bottom flanges near floor beam 3.
 - Span 6, girder 2, exterior face horizontal splice near floor beam 12 (photo 27).
 - Span 7, girder 1, exterior face horizontal splice near floor beam 3.
- **FX** Longitudinal stiffeners on the exterior face of the girders have been retrofitted with a cored hole made through the stiffener and tangent with the girder web at the butt weld locations noted below. The stiffeners exist within the compression zones of the girder and the deck is not noted as composite with the girders.
 - Span 5, girder 1 between floor beams 4 and 5 at the lower longitudinal stiffener A
 1 1/4-inch-long vertical paint crack exists in the girder web at the cored hole
 location in the lower longitudinal stiffener (photo 28). The paint crack was

- observed during the 2021 fracture critical inspection is now defined with corrosion along the crack. Magnetic particle testing was not performed on the crack during either inspection.
- Span 6, girder 1 near floor beam 6 at the upper longitudinal stiffener A paint crack exists in the free edge of the stiffener.
- Span 6, girder 1 near floor beam 7 at the upper longitudinal stiffener Crack in the free edge of the stiffener (photo 29).
- o Span 6, girder 1 near floor beam 9 at the upper longitudinal stiffener.
- o Span 6, girder 2 near floor beam 9 at the upper longitudinal stiffener.
- o Span 7, girder 2 between floor beams 7 and 8 at the lower longitudinal stiffener.
- **FX** Span 7, girder 1 web between floor beams 3 and 4 exhibits a global bow up to 1/2-inch at the field splice. No signs of distress were noted to the splice plates or bolts.
- Girders top flange exhibit surface corrosion and 1/8-inch-thick pack rust between the flange and soffit in various locations.
- Painted over pitting was observed in the web of the girders adjacent to the top of lower lateral bracing gusset plates. This deterioration is most likely due to debris build up capturing moisture. No active pitting was noted.
- Pack rust up to 1/2 inch thick has developed between the horizontal web splice of the girders causing distortion at several locations (photo 30). This condition does not affect the load carrying capacity of the girders.
- Pack rust up to 5/16 inch thick exists at isolated locations at the bottom flange splice plates.
- Heavy laminating corrosion was noted at the girder horizontal splices at the bearing stiffeners over piers 5 and 6. Girder 2 over pier 6 exhibits additional section loss greater than 50% to 4 of 6 bolts.
- Pack rust and section loss up to 3/16 inch deep exists in the girders top flange at several of the deck joints.

Multi girder spans exist in spans 1 through 4 and 8 through 15 and have the following comments:

- **FX** Isolated cross frame top struts exhibit cracked welds between the cross frame and gusset plate due to pack rust. The following locations exhibited cracks:
 - Cross frame at pier 1, connection to girder 3 5 3/8-inch-long crack in the bottom weld.
 - \circ Cross frame at pier 3, connection to girder 4 1/4-inch-long crack in the top weld.
 - Cross frame at pier 4, span 4 connection to girder 1 1/4-inch-long crack in the top weld and a broken weld at the bottom weld connection for the top strut (photo 31).
 - Cross frame at pier 12, connections to girders 2 and 3 crack full length of the gusset plates due to pack rust (photos 32 and 33).
- Pack rust up to 1 1/4 inches thick is typical between the girder cross frame members and vertical web and bearing stiffeners. Minor to moderate pitting and distortion to the gusset plate is also present at these locations (photo 34).

• Girder cross frames between girders 1, 2, and 3 at pier 9 and pier 10 exhibits a 3-inch bow, most likely due to the bearing rehabilitation project.

• Span 15, girder 1 at pier 14 exhibits a 1 3/4-inch-long crack in the vertical fillet weld to the exterior face of the girder web at the bottom flange. A 19-inch-long paint crack extends from this crack in the vertical fillet weld. These cracks appear to be contained within the fillet weld and do not extend into the base metal of the girder web.

Stringers – (5 = Fair condition)

- **PX** Loose stringer connection bolts were observed between the connection angle and the floor beam web at the following locations:
 - Span 5, stringer 2 at floor beam 4 1 loose bolt (photo 35)
 - Span 5, stringer 3 at floor beam 4 1 loose bolt
 - Span 5, stringer 3 at floor beam 8 1 loose bolt
 - Span 6, stringer 1 at floor beam 3 4 loose bolts
 - Span 6, stringer 2 at floor beam 3 1 loose bolt
 - Span 6, stringer 3 at floor beam 4 1 loose bolt (photo 36)
 - Span 6, stringer 1 at floor beam 5 2 loose bolts
 - Span 6, stringer 1 at floor beam 6 2 loose bolts
 - Span 6, stringer 2 at floor beam 6 1 loose bolt
 - Span 6, stringer 3 at floor beam 6 3 loose bolts
 - Span 6, stringer 3 at floor beam 8 3 loose bolts
 - Span 6, stringer 1 at floor beam 11 5 loose bolts
 - Span 6, stringer 1 at floor beam 12 1 loose bolt
 - Span 7, stringer 3 at floor beam 4 1 loose bolt (photo 37)

The bolts appear to have not been properly tightened during construction with most locations being the result of improper fit or alignment. These loose bolts do not provide the clamping strength intended for the connection and rely on bearing against the bolt shank for strength.

- **FX** Stringer connection angles welded to the replaced floor beams exhibit cracks in the bottom weld at the following locations:
 - \circ Span 5, stringer 3 connection to the east face of floor beam 3 3 1/2-inch-long crack (1/2 inch increase since the previous inspection) (photo 38).
 - Span 7, stringer 1 connection to the east face of floor beam 0 − 1 3/4-inch-long crack.
 - Span 7, stringer 3 connection to the east face of floor beam 0 1-inch-long crack (photo 39).
- Span 7, stringer 3 at floor beam 0 has been repaired by removing the deteriorated end and welding in a new steel section.
- Multiple stringers exhibit mis-drilled holes in the bottom flange at the floor beam connections.

[FCM] Floor Beams – (5 = Fair condition)

The floor beams in the twin girder spans (spans 5 through 7) act effectively as trusses. The diagonal and vertical floor beam members carry the stringer loads to the girders. The floor beam at each deck joint acts as an end diaphragm with the stringers framing into the face of the floor beam. These members exist at floor beams 0, 3, and 6 in span 5, floor beams 0, 3, 6, 8, and 11 in span 6, and floor beams 0, 3, 6, and 9 in span 7. The floor beam truss gusset plates are welded to the bottom flange of the floor beam upper chord beneath each stringer. The upper chord of the floor beams not under deck joints are significantly shallower with the stringers bearing on the top of the member. For the purpose of this report, the floor beams are considered to act as a truss and the components contain typical truss element descriptions.

- PX Span 5, west face of floor beam 6 at girder 1 exhibits a 5 1/8-inch-long crack in the
 weld for the web connection plate due to pack rust (photo 40). This represents an
 increase of 5/8 inch since the previous inspection. The weld is 15-inches-long and occurs
 along both faces of the floor beam web. Deck drainage leaking though the deck control
 joint is the source of the pack rust.
- **PX Member Alignment** Span 6, floor beam 0 over pier 5 at girder 2 is cracked for the full width of the horizontal weld along the bottom edge of the truss floor beam gusset plate **(photo 41)**. The vertical weld at this location is cracked full height (3 1/2 inches). The gusset plate has been reinforced with a welded 3-inch by 1/2-inch diagonal bar which is bowed out-of-plane 1/16 inch **(photo 42)**. This bow may be indicative of a recent overload especially with the multitude of previously undocumented bows in adjacent gusset plates.
- **PX** Loose and misaligned bolts and blind holes exist in the floor beam to girder connections at the following locations:
 - Span 5, floor beam 0 upper connection to girder 1 2 bolts not fully seated.
 - Span 6, floor beam 1 lower connection to girder 1 11 loose bolts (photo 43).
 - \circ Span 6, floor beam 4 lower connection to girder 1 2 blind holes at the top of the gusset plate with adjacent pack rust up to 11/16-inch-thick (photo 44).
 - Span 6, floor beam 5 lower connection to girder 2 2 blind holes (photo 45).
 - Span 6, floor beam 12 lower connection to girder 1 1 unseated bolt due to misaligned holes.
 - \circ Span 6, floor beam 13 lower connection to girder 1 4 loose bolts and one bolt without a nut allowing active pack rust up to 1/4 inch thick at the loose bolts.
 - Span 7, floor beam 2 lower connection to girder 1 1 missing bolt.
 - Span 7, floor beam 3 upper connection to girder 2 3 loose bolts and one bolt without a washer (photo 46).
 - Span 7, floor beam 9 upper connection to girder 1 2 missing bolts.
- **FX** The following floor beams have been replaced as of the 2014 OS:
 - Span 5, floor beam 3.
 - o Span 6, floor beam 0.
 - Span 7, floor beam 0.

The stringer to floor beam connections and the girder to floor beam connections at these locations are welded which differ from the details in Sheet 16 of the repair plans which call for bolted connections (photo 47). Many of the welds in these locations have irregular weld contour. Floor beam 0, span 6 over pier 5 – east face of floor beam, south face of

stringer 1 toe weld between the connection angle and the floor beam web exhibits a 3/4-inch possible crack. It is possible this is a fold in an uneven weld due to poor weld contour and not a crack.

- Span 7, floor beam 0 exhibits a previous repair at girder 2 with the floor beam reattached to the girder via welded plate prior to the 2014 OS inspection. The weld has 1 1/8-inchlong and 1/2-inch-long cracks at the lower end of the weld (photo 48). This retrofit plate is positioned to resist the vertical dead load reaction of the lower strut and is not well suited to resist the axial load the bottom strut was intended to carry.
- Member Alignment Several kinks and bends were noted in the floor beam members
 and gusset plates. It was unable to be determined at the time of the inspection if this is an
 as-built condition or if this is the result of recent damage due to overload; however, the
 lack of fatigue or crack indications suggests that the kinks are an as-built condition. Details
 and locations are as follows:
 - o Span 5, floor beam 2 at girder 2 L4 gusset plate exhibits a slight bow.
 - Span 5, floor beam 5 at girder 2 L4 gusset plate exhibits a slight bow.
 - Span 5, floor beam 7 adjacent to girder 2 U3 gusset plate exhibits an approximately 3/8-inch kink under stringer 3 and L4 gusset plate exhibits an approximately 1/8-inch bow.
 - Span 6, floor beam 4 Center gusset plate kinked.
 - Span 6, floor beam 13 LOL1 exhibits 2 minor kinks.
 - Span 7, floor beam 1 at stringer 3 upper chord bottom flange is twisted/rolled 7° to the east. The upper gusset plate under stringer 3 is kinked 1/2 inch on the vertical edges and 1/2 inch on the bottom horizontal edge. The vertical stiffeners are out of alignment due to the roll in the bottom flange of the floor beam. The center gusset plate is kinked 1/4 inch to the west (photo 49).
 - Span 7, floor beam 5 upper chord is rotated 4.5° to the east (photo 50).
 - Span 7, floor beams 2, 5, and 8 at stringer 3 bottom horizontal face of gusset plate kinked 1/4-inch and rotated up to 1/2-inch to the west. Floor beam 2 exhibits a poor-quality weld between the north vertical stiffener under stringer 3 and the floor beam bottom flange that appears to have never properly been attached at this location.
- Span 6, floor beam 2 U3L2 (tension member) exhibits several shallow gouges up to 3/8-inch-deep in the bottom flange.
- Span 6, floor beam 4 exhibits two mis-drilled holes in the bottom flange under stringer 3.
- Span 6, floor beam 6 top flange exhibits a 14-inch by 1-inch corrosion hole with adjacent knife edging.
- Oversized holes exist randomly throughout the floor beam connections. The holes appear
 to have been re-drilled during the erection of the bridge. The bolt holes are close to the
 top edge of the connection plate, reducing the capacity of the connection. No signs of
 distress were observed and the connection most likely is adequate.
- Several floor beams exhibit surface corrosion along the top flange with evidence of deck pumping due to splash marks on the underside of the deck.

• The floor beams typically exhibit corrosion on both flanges and up to 1/8-inch-deep pitting on the bottom face of the top flange.

Floor Bracing System – (5 = Fair condition)

- **PX** Span 5, lower lateral bracing diagonal east of floor beam 7 and at girder 2 exhibits a 5-inch-long crack in the weld between the bottom angle and the bracing gusset plate caused by active pack rust between the diagonal and the lower lateral bracing gusset plate **(photo 51)**.
- **PX** Span 6, lower lateral bracing diagonal east face of floor beam 12 and at girder 2 exhibits a 5 3/4-inch-long crack in the weld between the bottom angle and the bracing gusset plate caused by active pack rust between the diagonal and the lower lateral bracing gusset plate **(photo 52)**.
- Span 5, lower lateral bracing diagonal east of floor beam 1 at girder 2, exhibits a crack along the end of the bracing due to pack rust (photo 53). The bracing is welded along the west edge and end of the bracing.
- Many lower lateral bracing hanger rod connections were replaced prior to the 2014 OS inspection although the hanger rod to stringer connections do not include lock washers as detailed in the repair plans. In many locations the bolted assembly is not tight allowing the connection clamp to slide along the stringer bottom flange. Several other hanger rods remain severed. In other locations the lower lateral bracing connection brackets to the stringers are missing (photo 54). These rods prevent oscillation of the lower lateral bracing under live loads. Oscillation of the lower lateral bracing can cause fatigue cracks in the gusset plate weld to the web of the girders.
- Previous recommended repairs for lower lateral bracing welded angles were performed prior to the 2014 OS inspection. Pack rust has been removed and angles have been welded on two of three legs at most locations, as well as all three legs at random locations.
- The lower lateral bracing crossbuck connections between floor beams exhibit broken welds at the following locations due to pack rust forming between the flange of the diagonal member and the gusset plates:
 - Span 5, between floor beams 0 and 1 southwest diagonal member at the gusset plate connection.
 - Span 6, between floor beams 10 and 11 northeast diagonal member at the gusset plate connection (photo 55).
 - Span 7, between floor beams 3 and 4 southeast diagonal member at the gusset plate connection, exhibits a cracked weld full flange width (photo 56).
- Span 6 lower lateral bracing between floor beams 3 and 4 exhibit up to 1-inch-thick pack rust between the gusset plate and the floor beam causing the bracing to rotate.
- Span 7 lower lateral bracing gusset plate at floor beam 6 exhibits a 5-inch by 2-inch corrosion hole through the gusset plate at the edge of the floor beam connection stiffener to girder 1.

Paint/Coating System – (6 = Satisfactory condition)

The bridge was repainted in 2010. Areas of previous corrosion and pack rust are
reactivating in many locations especially at gusset plates near the expansion joints. Pack
rust is active in many girder horizontal web splices. Previous PX of laminating corrosion
and pack rust at lower lateral bracing gusset plates were repaired prior to the 2014 OS
although corrosion is reactivating in isolated locations.

Load Deflection – (4 = Poor condition)

The approach spans were observed to oscillate and have noticeable deflection during the
passage of multiple loaded trucks. Additionally, the approach span piers exhibited
longitudinal oscillations during these passages. These conditions may be caused by the
deck lifting at the control joints over intermediate floor beams, creating a ramping effect
and magnified impact loading on the superstructure.

NBI Item 60 – Substructure (6 = Satisfactory condition)

Abutments – (6 = Satisfactory condition)

- The bottom of both abutment breastwalls are exposed up to 2 inches high by 4 feet wide at both ends with up to 30 inches of penetration (photo 57). The steel piles are not exposed.
- The backwalls appear to be leaning towards the channel. A level was used to confirm that
 the girder ends remain near vertical, and the backwalls are leaning towards the channel.
 Abutments are supported on vertical piles. Measurements between the backwall and the
 girder top and bottom flanges were taken at the following locations:
 - The west abutment transverse measurement between the abutment backwall and the girder flanges at span 1, girder 4 are 4 7/8 inches at the top flange (previously 1 inch) and 7 inches at the bottom flange (previously 3 1/4 inches) (photo 58).
 - The east abutment transverse measurement between the abutment backwall and the girder flanges at span 15, girder 4 are 1 1/8 inches at the top flange and 3 1/4 inches at the bottom flange (photo 59).
- The west abutment exhibits varmint holes under the breastwall between girders 3 and 4.
- West abutment bearing seats exhibit light accumulation of spalled concrete and debris (photo 60).
- The east abutment exhibits a 7-foot-wide patched area between girders 2 and 3 and a horizontal crack with rust staining near the girder 3 pedestal. Moist sand from the epoxy overlay exists on the abutment seat.

Piers – (6 = Satisfactory condition)

- Pier 1 cap exhibits an incipient corner spall/delamination along the east edge near girder 3
 (photo 61).
- Pier 2 cap exhibits a 3/16-inch-wide crack along the east and west edges near girder 2 and the top face of the cap in this area is delaminated. Cracking and delaminations are due to corrosion of the reinforcing steel.

• Pier 3 cap exhibits 1/16-inch-wide cracks in the top face with large, delaminated areas. The web wall has multiple shallow spalls with exposed reinforcing in the west face.

- Pier 4 cap exhibits spalling and scaling concrete with exposed corroded reinforcing steel in the bearing seat areas and to the west face over the north column. Scaling concrete 1/8-inch-deep exists around the bearing for girder 1, span 5 (photo 62).
- The south column of pier 4 exhibits cracking with efflorescence on the east face (photo
 63).
- The west face of the pier 5 cap at the interface with the column exhibits multiple exposed and corroding reinforcing steel ends (photo 64). Pier 5 also exhibits random hairline shrinkage cracks and isolated areas of small delaminations.
- The column of pier 6 exhibits random full height vertical cracks with light efflorescence and full width spalling with exposed reinforcement at the cross-section change near the waterline.
- Pier 7 cap exhibits map cracks in the patched areas and spalling with exposed reinforcement around the base of the north column.
- Pier 8 cap exhibits 1/16-inch-wide by 5-foot-long longitudinal cracks along the west and east top edges at girders 1 and 2 and delaminated concrete. Cracking and delaminations are due to corrosion of the reinforcing steel.
- The north column of pier 8 exhibits multiple spalls with exposed reinforcement.
- Pier 11 web wall exhibits multiple spalls with exposed reinforcement.
- Pier 13 cap exhibits longitudinal cracks along the edges under girders 1 and 2.
- Pier 14 cap exhibits 1/16-inch-wide cracks on the top face with large delaminated areas. Spalling and scaling concrete with exposed corroded reinforcing steel exists in the bearing seat areas and on the south face (photo 65).

Bearings - (5 = Fair condition)

- **PX** Bearing anchor bolts and fasteners exhibit the following conditions:
 - Pier 2, girder 4 bearing One loose anchor bolt.
 - Pier 3, girder 1 bearing Fixed bearing anchor bolts are bent and exhibit corrosion (photo 66).
 - Pier 5, girder 1 bearing Fixed bearing exhibits several different length anchor bolts, and the bolts are typically not fastened tightly. This possibly is the result of the anchor bolts working up out of the bearing seat due to rocking of the fixed bearings (photo 67).
 - Pier 8, girder 2 bearing Fixed bearing exhibits one missing anchor bolt at the southwest corner of the bearing.
 - Pier 9, girder 1 bearing Fixed bearing is missing one anchor bolt at the southwest corner of the bearing with the remaining 3 bolts exhibiting nuts not completely threaded onto the bolt. The southwest anchor bolt for the sole plate connection to the bottom flange is loose (photo 68).
 - Pier 11, girder 4 bearing One loose anchor bolt at the southwest corner with no signs of movement.

 Pier 12, girder 4 bearing – East anchor bolts are not fully seated and are slightly bent to the east.

- East abutment, girder 4 bearing Anchor bolts exhibit up to approximately 20% loss to bolt heads due to corrosion.
- The keeper plates used to contain the rocker bearing within the limits of the sole plate have broken welds or is missing at the west abutment bearings for girders 3 and 4 (photo 69). The girder 4 bearing has moved south 1/2 inch with no significant lateral movement since the last painting.
- Fixed bearings typically exhibit surface corrosion forming at stiffeners and masonry plates and minor pack rust developing between the masonry plate and concrete bearing seat.
- Pier 10, girder 1 bearing has rotated clockwise (looking down), and the southwest (span 9 side) corner of the rocker overhangs the masonry plate 1/4 inch (photo 70).
- The rocker bearings typically exhibit rust staining and active laminating corrosion between the rocker and the masonry plate.
- Previous rocker bearings for span 4 at pier 4, span 8 at pier 7, and span 11 at pier 10 have been replaced with elastomeric bearings prior to the 2014 OS inspection.
- Bearing measurements are listed in the table below (photos 71 and 72).

Pier	Average Rotation/ Translation	Max Rotation or Translation	Direction	Expansion/ Contraction	Temperature
Spans 1 thr	ough 4 - four spa	n continuous 4-	girder approa	ich spans	
West abutment	4°	7°	West	Expansion	90°F
Pier 1	0°	0°	-	-	86°F
Pier 2	Fixed	-	-	-	
Pier 3	Fixed	1	-	-	
Pier 4	0"	3/4"	West	Contraction	85°F
Spans 5 t	hrough 7 - three :	span continuous	2-girder mai	n spans	
Pier 4	8°	8°	East	Contraction	85°F
Pier 5	Fixed	1	-	-	
Pier 6	5°	7°	East	Expansion	85°F
Pier 7	3°	3°	-	Expansion	96°F
Spans 8 thro	ough 10 - three sp	an continuous 4	l-girder appro	ach spans	
Pier 7	0"	0"	-	-	80°F
Pier 8	Fixed	ı	-	-	
Pier 9	Fixed	1	-	-	
Pier 10	6°	9°	West	Contraction	77°F
Spans 11 thr	ough 14 - four sp	an continuous 4	l-girder appro	ach spans	
Pier 10	1/2"	1"	West	Contraction	77°F
Pier 11	fixed	-	-	-	

Pier	Average Rotation/ Translation	Max Rotation or Translation	Direction	Expansion/ Contraction	Temperature
Pier 12	fixed	-	ı	-	
Pier 13. G2,3,4	2°	3°	East	Expansion	95°F
Pier 13, G1	4°	4°	West	Contraction	95°F
Pier 14. G 2,4	2°	2°	East	Expansion	80°F
Pier 14. G 1,3	4°	8°	West	Contraction	80°F
Span 15 - simple span 4-girder app		irder approach s	span		
Pier 14	12°	14°	West	Expansion	95°F
East abutment	Fixed	-	-	-	

NBI Item 61 – Channel and Channel Protection (6 = Bank Slumping condition) *NBI Item 61 was* rated 6=Bank Slumping condition during the October 14, 2022 underwater inspection. The following conditions are based on observations during the 2023 fracture critical inspection.

Flowline Stability – (7 = Good condition)

No significant deficiencies noted.

Channel Bank Damage – (7 = Good condition)

• No significant deficiencies noted.

Debris – (6 = Satisfactory condition)

• As per the 2022 underwater inspection, light timber debris exists on the riverbed at piers 3, 4 and 7 through 10.

Vegetation – (7 = Good condition)

• The banks are sandy and well vegetated with grass and tree growth on both banks.

NBI Item 72 – Approach (7 = Good condition)

Approach Roadway Condition – (7 = Good condition)

- Both approach slabs have been recently replaced. The east and west approach slabs exhibit up to 0.020-inch-wide longitudinal cracking in the wheel lines with intersecting transverse cracks (photo 73).
- The west approach slab approximately 40 feet from the west abutment exhibits a 7 1/2-inch diameter infilled core hole in the west travel lane (photo 74).
- A spall measuring 2 feet by 6 inches exists along the east abutment joint.
- Pavement relief joints at the ends of both approach slabs exhibit adhesion failures and minor debris impaction.

Approach Roadway Settlement – (7 = Good condition)

• No settlement issues were noted at the time of the inspection.

NBI Item 113 – Scour Rating (8 = Calculated Scour Above Foundation) No change to scour rating is recommended.

• Per the 2022 Underwater Inspection report: There has been general scour ranging from 5-ft to 15-ft, west of Pier 7 since construction. The top of the footing at Pier 5 and Pier 6 is exposed; however, the footings are keyed into hard shale, according to the design plans.

Truss/FC Bridge Rating Form

NBI	
Structure	5159 0300X
County	Muskogee
Division	1

Flowline/Notes

Facility Carried			
S.H. 100			
Feature Intersected			
Arkansas River			

N/A

N/A

Structure 5159 0300X	Э.П.	100
County Muskogee	Feature Intersected	
Division 1	Arkansas	River
	<u> </u>	
NBI Item #	2023	2021
	- DV	- DV
36 - Traffic Safety	5, PX	5, PX
58 - Deck	6, PX	6, PX
a. Driving Surface	6, PX	6, PX
b. Soffit	6, FX	6, FX
c. Joints	6, PX	6, PX
0.00	0 ,174	0,12
59 - Superstructure*	5, PX	5, PX
a. Beams/Girders	5, PX	5, PX
b. Stringers**	5, PX	5, PX
c. Floor Beams	5, PX	5, PX
d. Pier Beams	N/A	N/A
e. Floor Bracing System	5, PX	5, PX
f. Truss Upper Chord***	N/A	N/A
g. Truss Lower Chord***	N/A	N/A
h. Truss Web Members	N/A	N/A
i. Truss End Posts	N/A	N/A
j. Truss Bracing	N/A	N/A
k. Paint/Coating	6	6
I. Load Deflection	4	4
00 0 1 4 4 4444	0.00	0 DV
60 - Substructure****	6, PX	6, PX
a. Abutments	6	6, FX
b. Piers	6	6
c. Bearings	5, PX	5, PX
61 - Channel & Channel Protection	6	6
a. Flowline Stability	7	7
b. Channel Bank Damage	7	6
c. Debris	6	7
d. Vegetation	7	7
Approach Roadway	7	7
a. Approach Roadway Condition	7	7
b. Approach Roadway Settlement	7	7
113 - Scour	0	0
113 - 300ur	8	8
	N1/5	

Rating	Description (For 36, 58, 59, 60, 72)
N/A	NOT APPLICABLE
9	EXCELLENT CONDITION
8	VERY GOOD CONDITION - no problems noted.
7	GOOD CONDITION - some minor problems.
6	SATISFACTORY CONDITION - structural elements show some minor deterioration
5 (FX,PX)	FAIR CONDITION - all primary structural elements are sound but may have minor section loss, cracking, spalling or scour.
4 (PX)	POOR CONDITION - advanced section loss, deterioration, spalling or scour.
3 (PX,CX)	SERIOUS CONDITION - loss of section, deterioration, spalling or scour have seriously affected primary structural components. Local failures are possible. Fatigue cracks in steel or shear cracks in concrete may be present.
2 (CX)	CRITICAL CONDITION - advanced deterioration of primary structural elements. Fatigue cracks in steel or shear cracks in concrete may be present or scour may have removed substructure support. Unless closely monitored it may be necessary to close the bridge until corrective action is taken.
1 (CX)	IMMINENT FAILURE CONDITION—major deterioration or section loss present in critical structural components or obvious vertical or horizontal movement affecting structure stability. Bridge is closed to traffic but corrective action may put back in light service.
0	FAILED CONDITION - out of service - beyond corrective action.

- * Members with fatigue cracks in compression zones (top flange stringer copes, clip angles, etc.) are to be coded as a 5 unless the crack turns toward a tension zone, then code 3.
- * Members with fatigue cracks in tension zones (cover plate ends, etc.) are to be coded as a 3.
- ** Includes connection angles.
- *** Includes gusset plates. Missing rivets in connections are coded as a 3.
- **** Elements with superficial cracking are coded as 6, spalls with exposed rebar 5, spalls with exposed rebar with section loss 4.

Rating	Description (For 61)
N/A	NOT APPLICABLE
9	There are no noticeable or noteworthy deficiencies which affect the condition of the channel.
8	Banks are protected or well vegetated. River control devices such as spur dikes and embankment protection are
	not required or are in a stable condition.
7	Bank protection is in need of minor repairs. River control devices and embankment protection have a little minor damage. Banks and/or channel have minor amounts of drift.
6	Bank is beginning to slump. River control devices and embankment protection have widespread minor damage. There is minor stream bed movement evident. Debris is restricting the channel slightly.
5	Bank protection is being eroded. River control devices and/or embankment have major damage. Trees and brush restrict the channel.
4	Bank and embankment protection is severely undermined. River control devices have severe damage. Large deposits of debris are in the channel.
3	Bank protection has failed. River control devices have been destroyed. Stream bed aggradation, degradation or lateral movement has changed the channel to now threaten the bridge and/or approach roadway.
2	The channel has changed to the extent the bridge is near a state ofcollapse.
1	Bridge closed because of channel failure. Corrective action may putback in light service.
0	Bridge closed because of channel failure. Replacement necessary.





Photograph 1 - Looking east at the bridge end view.

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Photograph 2 - Looking north at the bridge elevation.

Photograph 3 - Looking northwest at the north rail east end post. Note: rail post is missing all four anchor bolts.



Photograph 4 - Looking northeast at the north bridge railing in span 6 neat pier 6. Note: corrosion hole through rail.



Photograph 5 - Looking west along the northeast approach railing. Note: the blockouts have been damaged for 60 feet near the transition.



Photograph 6 - Looking southwest at the south bridge railing in span 14. Note: top coat of paint is peeling due to adhesion failure.



Photograph 7 - Looking northwest at the north concrete curb at mid span of span 3. Note: 7-foot-long by full curb height spall with exposed and corroded reinforcing steel.



Photograph 8 - Looking west at the northeast approach railing transition. Note: transition meets current standards; however, safety curb extends 14 inches from face of railing and is unprotected.

Photograph 9 - Looking east along the south curb in span 10. Note: isolated scuppers clogged with debris. Moderate debris exists along edge of deck full length.



Photograph 10 - Looking northwest at span 7 deck top eastbound lane. Note: 2-foot-long by 1-foot-wide by up to 3-inch deep pothole with 5 exposed and corroded transverse reinforcement.



Photograph 11 - Looking north at span 5 top of deck. Note: transverse cracking spaced 1 to 3 feet apart.





Photograph 12 - Looking northwest at span 7 deck top. Note: typical patching in good condition throughout the bridge.

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Photograph 13 - Looking northwest at the deck near mid span of span 14. Note: concrete patches throughout with isolated asphalt patches and spalling.



Photograph 14 - Looking west at span 12 north soffit overhang near pier 12. Note: typical spalling with exposed and corroded reinforcement.



Photograph 15 - Looking east at floor beam 3, span 7. Note: pack rust and section loss exists along the top flange of the floor beam. Spalls are typical in the deck soffit adjacent to the floor beam.



Photograph 16 - Looking north along the sealed expansion joint at the west abutment. Note: moderate debris impaction throughout.

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Photograph 17 - Looking north along the finger joint over pier 4. Note: 5 feet of missing fingers on span 4 side in east travel lane, 4 feet missing in span 4 side near the north shoulder. Heavy debris compaction for the full length inhibits expansion of joint.



Photograph 18 - Looking north along the underside of the finger joint over pier 7. Note: trough torn and falling through along the underside.

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Photograph 19 - Looking north along the construction joint over floor beam 2 in span 3. Note: typical condition, isolated spalls/delaminations with concrete and AC patches.

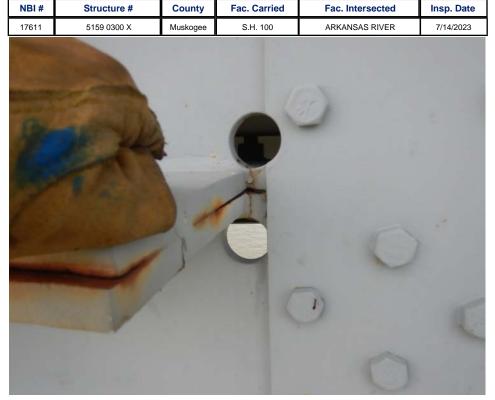


Photograph 20 - Looking southeast at girder 1, span 5 at the field splice near floor beam 5. Note: 5/8-inch-long crack in the inboard face at the horizontal web splice termination.

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Photograph 21 - Looking northeast at girder 2, span 5 at the field splice near floor beam 5. Note: 3/8-inch-long paint crack in the inboard face at the horizontal web splice termination.



Photograph 22 - Looking north at girder 1, span 6 at the field splice near floor beam 3. Note: 3/4-inch-long crack in the inboard face at the horizontal web splice termination has not propagated past the arrestor holes.

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Photograph 23 - Looking north at girder 2, span 6 at the field splice near floor beam 11. Note: 3/16-inch-long crack in the inboard face at the horizontal web splice termination.





Photograph 24 - Looking southwest at girder 1, span 7 at the field splice near floor beam 4. Note: 1-inch-long paint crack in the upper web with an arrestor hole, and a 1 1/8-inch-long paint crack in the lower web without an arrestor hole in the inboard face at the horizontal web splice termination.

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Photograph 25 - Looking south at girder 2, span 7 at the field splice near floor beam 4. Note: no cracks in outboard face of girder web



Photograph 26 - Looking up along the outboard face of the bearing stiffener for girder 1 at pier 6. Note: 1 missing bolt in horizontal splice. Corrosion and pitting exist at the splice interface.



Photograph 27 - Looking north at the span 6, girder 2 field splice near floor beam 12. Note: 1 missing bolt in the horizontal splice.



Photograph 28 - Looking north at girder 1, span 5 at the lower longitudinal stiffener splice between floor beams 4 and 5. Note: 1 1/4-inch long vertical paint crack in the girder web.

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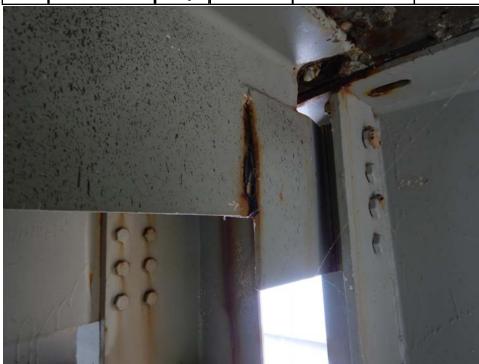


Photograph 29 - Looking north at girder 1, span 6 at the upper longitudinal stiffener splice near floor beam 7. Note: crack in splice on free edge side of cored hole.



Photograph 30 - Looking south along the girder 1, span 7 horizontal splice. Note: 1/4-inch-thick pack rust exists between the splice plates.





Photograph 31 - Looking southeast at the end diaphragm connection to girder 1, span 4 at pier 4. Note: pack rust has broken the bottom and vertical welds.



Photograph 32 - Looking north at cross frame connection to girder 2 over pier 12. Note: full-length crack in gusset plate to cross frame connection due to pack rust.



Photograph 33 - Looking south at cross frame connection to girder 3 over pier 12. Note: crack in gusset plate to cross frame connection due to pack rust.



Photograph 34 - Looking southwest at the diaphragm connection to girder 1 over pier 9. Note: typical pack rust between bearing stiffener and diaphragm interface up to 3/4 inch thick.





Photograph 35 - Looking north at the stringer 2 connection to floor beam 4, span 5. Note: bolt on east face is loose and bolt holes punched in wrong location.

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Photograph 36 - Looking southeast at the stringer 3 connection to floor beam 4, span 6. Note: loose bolt stringer connection bolt.

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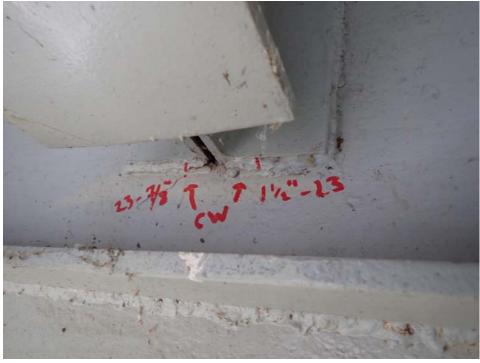


Photograph 37 - Looking east at the stringer 3 connection to floor beam 4, span 7. Note: one missing stringer connection bolt.



Photograph 38 - Looking west at the stringer 3 connection to floor beam 3, span 5. Note: 3 1/2-inchlong crack along weld on the underside of the stringer connection angles.

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Photograph 39 - Looking west at the stringer 3 connection to floor beam 3, span 7. Note: 1 1/2-inch and 7/8-inch-long cracks in weld on the underside of the stringer connection angles.



Photograph 40 - Looking east at floor beam 6 connection to girder 1, span 5. Note: $5\,1/8$ -inch vertical crack in connection weld.

	NBI#	Structure #	County	Fac. Carried	Fac. Intersected	Insp. Date
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Photograph 41 - Looking east at floor beam 0 lower connection to girder 2 over pier 5. Note: full width crack along the floor beam to gusset plate weld on both faces.



Photograph 42 - Looking north at floor beam 0 lower connection to girder 2 over pier 5. Note: gusset plate has been reinforced with a diagonal bar, which is now bowing out of plane 1/16 inch.

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Photograph 43 - Looking east at floor beam 1, span 6 connection to girder 1. Note: loose bolts exist in the bottom strut connection to the girder. Several misdrilled holes exist in the connection.

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17611	5159 0300 X	Muskogee	S.H. 100	ARKANSAS RIVER	7/14/2023



Photograph 44 - Looking east at floor beam 4 span 6, connection to girder 1. Note: 2 blind holes exist in top of the connection plate of the bottom strut. Pack rust is forming between the vertical stiffener and the connection plate.

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Photograph 45 - Looking east at floor beam 5, span 6 conneciton to girder 2. Note: 2 blind holes at the top of the connection.



Photograph 46 - Looking east at floor beam 3, span 7 connection to girder 2. Note: 3 loose bolts and 1 missing washer.

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Photograph 47 - Looking northwest at stringer 1 connection to the east face of floor beam 0, span 6. Note: stringer connection angle has been rewelded along the bottom edge.



Photograph 48 - Looking northeast at the floor beam 0 lower strut connection to girder 2, span 7.

Photograph 48 - Looking northeast at the floor beam 0 lower strut connection to girder 2, span 7. Note: 1 1/8-inch-long crack in repair plate weld on the west face, 1/2-inch-long crack on the east face.



Photograph 49 - Looking south along the top chord of floor beam 1 in span 7 between the stringers. Note: top chord is rotated to the east, kink in upper gusset plate under stringer 3.



Photograph 50 - Looking northwest at floor beam 5, span 7 under stringer 3. Note: top chord/strut is rotated 4.5 degrees east.



Photograph 51 - Looking west at the lower lateral bracing connection at the east face of floor beam 7 and girder 2, span 5. Note: 5-inch-long crack in the weld between the bottom angle and the bracing gusset plate.



Photograph 52 - Looking west at the lower lateral bracing connection to floor beam 12 and girder 2, span 6. Note: 5 3/4-inch-long crack in weld between lower lateral bracing and gusset plate.



Photograph 53 - Looking southwest at the lower lateral bracing connection to floor beam 1 and girder 2, span 5. Note: bracing is welded along the west edge and end allowing pack rust to form and crack weld at end of bracing.



Photograph 54 - Looking southeast at the lower lateral bracing hanger rod in span 6, between floor beams 5 and 6. Note: missing clamp to stringer bottom flange.

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Photograph 55 - Looking southeast at span 6, lower lateral bracing crossbuck connection between floor beams 10 and 11. Note: 2 cracked welds on northeast member due to pack rust.





Photograph 56 - Looking southeast at span 7, lower lateral bracing crossbuck connection between floor beams 3 and 4. Note: cracked weld on southeast member due to pack rust.



Photograph 57 - Looking northeast at the east abutment. Note: deck drainage leaking on bearing seat. Minor spall along bottom edge of breastwall between girders 2 and 3. 18 inches of penetration noted between girders 2 and 3 with no significant undermining noted vertically.



Photograph 58 - Looking south at girder 4, span 1 at the west abutment. Note: backwall is leaning towards the channel with 4 7/8 inches clear to the girder end near the top flange and 7 inches clear near the bottom flange.

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Photograph 59 - Looking south at girder 4, span 15 at the east abutment. Note: backwall is leaning towards the channel with 1 1/8 inches clear to the girder end near the top flange and 3 1/4 inches clear near the bottom flange.



Photograph 60 - Looking southwest at the west abutment. Note: light accumulation of spalled concrete and debris on bearing seat.



Photograph 61 - Looking north at pier 1 cap east edge near girder 3. Note: 5-foot-long corner spall/delamination.

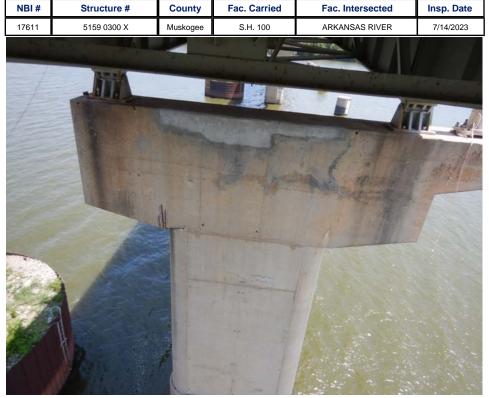


Photograph 62 - Looking north at pier 4 pier cap south end span 5. Note: scaling concrete around the girder 1 bearing.

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Photograph 63 - Looking west at pier 4, south column at the web wall interface. Note: cracking/spalling with efflorescence.



Photograph 64 - Looking east at pier 5. Note: patched area and spall with exposed reinforcing steel in cap due to deck drainage passing through previous deck control joint.

Photograph 65 - Looking north at the end of the pier 14 cap. Note: spalling and delaminations throughout the top of the cap.



NBI# Fac. Carried Insp. Date Structure # County Fac. Intersected S.H. 100 17611 5159 0300 X Muskogee ARKANSAS RIVER 7/14/2023

Photograph 66 - Looking west at girder 1, pier 3 bearing. Note: fixed bearing anchor bolts are bent.

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Photograph 67 - Looking southwest at the girder 1, pier 5 fixed bearing. Note: anchor bolt lifted and nuts not fully seated.



Photograph 68 - Looking northeast at girder 2 fixed bearing at pier 8. Note: missing anchor bolt.

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Photograph 69 - Looking west at the girder 4, span 1 expansion bearing at the west abutment. Note: south keeper plate attached to the sole plate is missing and the bearing has moved south 1/2 inch with no significant lateral movement since the last painting.

NBI#	Structure #	County	Fac. Carried	Fac. Intersected	Insp. Date
17611	5159 0300 X	Muskogee	S.H. 100	ARKANSAS RIVER	7/14/2023

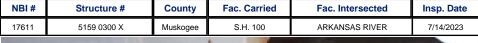


Photograph 70 - Looking south at the girder 1, span 10 expansion bearing at pier 10. Note: misalignment between the rocker and masonry plate with the rocker overhanging the masonry plate 1/4 inch.





Photograph 71 - Looking south at the girder 1, span 7 expansion bearing at pier 7. Note: bearing in expansion 3 degrees at 96F.

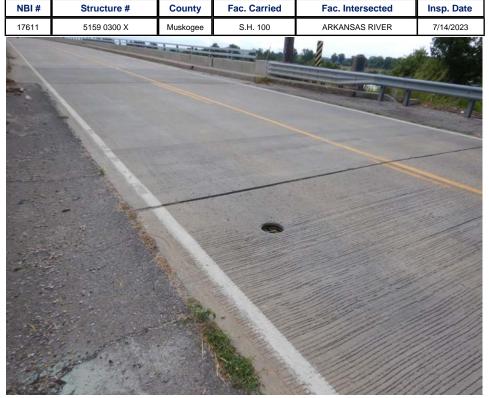




Photograph 72 - Looking north at the girder 1, span 10 expansion bearing at pier 10. Note: bearing is rocked 5 degrees in contraction at 77 F.



Photograph 73 - Looking southeast at the west approach slab in the eastbound lane. Note: longitudinal crack running the full length of the slab with intersecting transverse cracks.



Photograph 74 - Looking southeast at the west approach roadway. Note: 7 1/2-inch diameter filled core hole exists in the westbound lane approximately 40 feet from the west abutment.

		Dept. of Transporta		<u>'</u>
<u>NBI No.:</u> 17611	5159 0		<u>.ocal ID:</u> -1	Suff. Rating: 66.70
IDEN	TIFICATION	300 X	, 	INSPECTION
Bridge Description.	HICATION		Type Insp. Req	
4(100ft.CONT.) (207ft334ft207ft.CONT.)3(100ft.CONT.)	IT \4/100ft CON	IT \75# DI ATE	NBI:	1 24 months 7/14/2023 07/14/20
(2071)3341120711.CONT.)3(10011.COI	11.)4(1001t.CON	II.)/ SIL PLATE	FC: Y	1 24 months 7/14/2023 7/14/20
	,	S.H. 100	UW: Y	0 60 months 10/14/2022 10/14/20
2. Division: Division 1 6. Fe	-	RKANSAS RIVER	OS: Y	0 24 months 7/12/2022 7/14/20
3. County: MUSKOGEE 4. City: Unknown	9. S 11. Mile Post:	SEQUOYAH C/L 2.999 mi	40 Dana Lhuu Nati N	CLASSIFICATION
Admin Area: Unknown		/ Sub Rte: -1 / -1	I	ot on Base Network 101. Parallel Str.: No bridge exi 102. Traffic Dir.: 2-way traffic
5a. On/Under: Route On Structure	16. Latitude:	35° 31' 14.59"	20. Toll Facility: C 21. Custodian: State	In free road 102. Traffic Dir.: 2-way traffic 103. Temp. Str.: Not Applicable
5b. Kind of Hwy: State Hwy	17. Longitude:	095° 07' 24.89"	22. Owner: State	104. Hwy System: Not on NHS
5c. Lvl of Srvc: Mainline	98. Border	Unknown (P)		7 Rural Mjr Collecto 105. Fed Land Hwy: IRR-Indian Res
5d. Route No.: 00100	% Řesponsible		37. Historical Sig.: No	t eligible for NRHP 110. Defense Hwy: Not a STRAHNI
5e. Dir. Sufx: N/A (NBI)		g #: Unknown	100. Def. Hwy: Not a	a STRAHNET hwy 1112. NBIS Length: Long Enough
STRUCTURE TY				CONDITION
43a/b. Main Span:	•	Girder-Floorbeam	58.Deck: 6 Satisfac	, *
44a/b. Appr. Span:	2(66) /	Stringer/Girder	62.Culvert: N/A (NBI Flowline Notes:) 61.Chan./Chan. Prot.: 6 Bank Slumping
45. # of Main Spans: 3 46. # of Appr. Spans: 11				
46. # of Appr. Spans: 11 107. Deck Type: Concrete-Ca	ast-in-Place		1 1	eral scour ranging from 5-ft to15-ft, west of Pier 8 since of the footing at Piers 4, 5, 6, 8 and 9 are exposed;
108a. Wearing Surface: Epoxy Over			Construction. The top	or the rooting at Fiers 4, 5, 6, 6 and 9 are exposed;
108b. Membrane: None	-		1	LOAD RATING AND POSTING
108c. Deck protection: Unknown			ı	MS 18 (HS 20) Date Rated 11/24/2003
AGF A	ND SERVICE			A Open, no restriction 5 At/Above Legal Loads
19. Detour Length: 9.9 mi	106. Year Rec	onst.:	63.Op / 65.Inv. Rating	· · · · · · · · · · · · · · · · · · ·
27. Year Built: 1969	109. Truck AD	,		H HS 3-3 EV3 SHV
28a/b. Lanes on/und: 2 / 0			64. Operating Rating	(tons): 33.29 54.45 75.84 0.00 0.0
29. ADT: 3,300			66. Inventory Rating (tons): 19.95 32.63 45.53 -1.00
30. Year of ADT: 2020	l	•••		APPRAISAL
42a/b. Type of Svc on/und: Highway	' /	Waterway	36a. Brdg Rail: 0	Substandard 68. Deck Geom.: 4 Tolerable
GEOM	ETRIC DATA		36b. Transition: 1	Meets Standards 69. Vert./Horiz. Undclr: Not applica
10. Vert. Clearance: 99.99 ft	50a. Curb/Sdv		1 ''	Meets Standards 71. Waterway Adeq: 8 Equal Desi
32. Appr Rwy Width: 44.00 ft	50b. Curb/Sdv		36d. Appr.Rail Ends:	1 Meets Standard 72. Appr. Alignment: 6 Equal Min C
33. Median: No median 34. Skew: 0.00°	51. Width Curb		67. Str Evaluation:	5 Above Min Tolera 1113. Scour Critical: 8 Stable Above
35. Struct. Flared: No flare	Deck Area			PROPOSED IMPROVEMENT
47Horizontal CIr: 28.00 ft	53. Min.Vert.C		94. Bridge Cost:	\$11,530,195 75. Type of Work: 31 Repl-Load C
48. Length Max Span: 333.99 ft	54a.Min.Vt.Un	dclr.Ref. N Feature not hwy c	95. Roadway Cost: 96. Total Cost:	\$4,500,000 76. Lngth of Improvement: 1,928 114. Future ADT: 5,280
49. Struct. Length: 1,928.15 ft	54b. Min. Vert.		97. Yr.of Cost Est.:	2015 115. Yr. of Future ADT: 2040
	55a. Min.Lat.U	•		NAVIGATION DATA
	55. Min.Lat.Un		38. Nav. Control:	Permit Required
	56. Min.Lat.Un		39. Vert. Clearance:	52.0 ft 111. Pier Protect.: 2 In-Place, F
200c. Temperature: 99	OKLAHOM/	ATTEMS	40. Horiz. Clearance:	300.0 ft 116. Lift Bridge Vert. Clr.: 0.0 ft
200d. Weather: Clear	/	214a. Posted Weight Limit:	NR	244. Span Lengths: 100 100 100
ě .	36 / -1	b. Posted Speed Limit:	INIX	
202. Waterprf.Membrane: -1 Date Installed: 01/01/190	1	c. Narrow/1way Brdg Sign:	NA	100 207 334 207 100
203. Type Exp. Device: Finger	•	d. Vertical Clr. Sign:	NA	245. Girder Depth: 246a. Type of Ovelay: Chipseal
_		Adv. Warning Sign:	NA Vos	b. Overlay Thickness: 0.10
	uare hand rail	e. Navigation Lights?: Working/Not Working:	Yes Yes	c. Overlay Date: 05/01/2014
205. Material Quantity: -3.00 208a. Type of Abutment: Skeleton			ATE HIGHWAY	d. Ovly Depth Changed >1": N
b. Type of Found.: Steel Pilin	g	218. Functionally Obsolete :	-	247. Protective Systems:
209. Type of Pier/Found.: 2	/ No	220. Bridge Redecked	_	
Spread Fo		` ,	tisfactory Condition	
210. Foundation Elev.: 4,402.00	4,352.00	222. Fill Over RCB: 0	0	248. # Field Splices w/ Corrosion: 3 249. Scour Crit. POA Exists?:
1.00	-1.00	223. Appr.Slab/Rwy Cond.:	2 gania Zina(OZ E II) Cre	250. Headwall:
211. Wear.Surf.Prot.Sys: None	4	225. Paint Type/Ovrct: Org	ganic Zinc(OZ-E-U) Gra	258. Plans w/Found.in ODOT File
Date Installed: 01/01/190 211c. Silane Reapplied	I	226. Date Painted: 20		259. Scour Eval. in ODOT File:
211d. Date :		227. Paint Color: Gra		263. Interchange at Intersection: No
213. Utilities Attached: Communica	tion	233. Deck Forming:	-	264. Interstate Milepoint:
Natural Gas Power	uon		rrent & Desired route	
INALUIAI GAS FOWEI _		240. Appr. Rwy Type.: Co	ncrete	
	1	243. Grdr Spacing/No.:	1	

NBI N 1761		Structure 5159 030		Local ID: -1	<u>Suff. Rating:</u> 66.70	ND
Inspection Date:	7/14/23		Shaun Fillmore			
Invoice No.:	1098920	Inspected With:	Colton Powell			

BRIDGE NOTES:

15 span structure consisting of: Spans 1-4 100-foot long continuous steel multi girders spans; Spans 5-7 three span continuous steel twin girders (207 feet, 334 feet, 207 feet); Spans 8-10 three 100-foot long continuous steel multi girders spans; Spans 11-14 four 100-foot long continuous steel multi girders spans; Span 15 100-foot long simple steel multi girder span.

O/S Inspection items include:

- · Girder web cracks at:
- o Span 5, G 1 (south face) between FBs 4 and 5 1 1/4-inch paint crack in web at the longitudinal stiffener cored hole (perform Magnetic Particle Testing during 2022 O/S inspection)
 - o Span 5, G 1 at the field splice near FB 5 5/8-inch crack with no arrestor hole.
 - o Span 5, G 2 at the field splice near FB 5 paint crack.
 - o Span 6, G 1 at the field splice near FB 3 arrested crack.
 - o Span 6, G 2 near FB 11 3/16-inch crack.
 - o Span 7, G 1 at the field splice near FB 4 paint crack.
 - o Span 7, G 2 at the field splice near FB 4 arrested crack.
- Cracks in the stringer connection angles welds to replaced FBs at:
 - o Span 5, stringer 3 connection to FB 3
 - o Span 7, stringer 1 connection to FB 0
 - o Span 7, stringer 3 connection to FB 0
- · Crack on exterior face of span 15, beam 1 in near pier 14.
- · Cracked FB to girder connection welds:
 - o Span 5, FB 6 upper connection to G 1 5 1/8-inch crack in connection plate weld.
 - o Span 6, FB 0 lower connection to G 2 horizontal weld cracked full length.
 - o Span 7, FB 0 lower connection to G 2 1 1/8-inch and 1/2-inch cracks in welded repair.

INSPECTION NOTES: 7/14/23

Channel Notes: The channel in the vicinity of the bridge has a slight bend and is well aligned with the piers. There are spur dikes on the east bank (outside of the bend), approximately 450-ft, 1400-ft, and 2700-ft upstream of the bridge. Both embankments are protected with dense vegetation. The embankments appear stable. There is light to moderate timber debris on the channel bottom at Piers 3, 4, 7, 8, 9, and 10; however, there are no significant restrictions to flow at the bridge. The channel bottom material at the piers consists of sand, gravel, and rock.

UW Inspection General Notes: The submerged portions of the substructure are in satisfactory condition. There is light abrasion on the columns and webwalls ranging from 1/16-in deep to 1/8-in deep and algae growth.

PΧ

- · Replace N railing post anchor bolts missing at eastern most railing post.
- · Unclog deck scuppers.
- · Reseal fixed poured joint seal at both abutments.
- · Arrest girder web cracks at horizontal splice termination at:
- o Span 5, G 1 at field splice near FB 5 5/8 inch.
- o Span 6, G 2 near FB 11 3/16-inch-long vertical crack in lower web plate.
- Replace missing bolts and tighten loose bolts at
- o Girder splice locations
- o FB connection to girders in spans 5, 6 and 7.
- o Stringer connection to FBs in spans 5, 6 and 7.
- Repair cracked web connection plate weld for FB 6 in span 5 at G 1.
- · Reattach FB 0 lower connection to G 2 in span 6.
- Repair cracks in lower lateral bracing in span 5, FB 7, G 2 and span 6, FB 12, G 2.
- Tighten loose anchor bolts and replace missing or bent anchor bolts .

FX - Monitor

- Monitor deck soffit along girders, FBs and stringers for further spalling.
- Monitor vertical offset of finger joints for changes in height at piers 4 and 7.
- · Monitor locations of girder web cracks having drilled hole retrofits or paint cracks at horizontal splice termination at:
- o Span 5, G 2 at field splice near FB 5 paint crack.
- o Span 6, G 1 at field splice near FB 3 arrested crack.
- o Span 7, G 1 at field splice near FB 4 paint crack.
- o Span 7, G 2 at field splice near FB 4 arrested crack.
- Monitor 1 1/4-inch long paint crack in span 5, G 1 web at longitudinal stiffener cored hole between FBs 4 and 5 (Magnetic Particle Testing to be performed during 2022 O/S inspection).
- Monitor cored hole locations in longitudinal stiffeners for crack development in girder web .
- Monitor bow in web of G 1, span 7 at field splice between FBs 3 and 4.
- · Monitor cracked welds at cross frame connection to girders due to pack rust.
- Monitor cracks at stringer connection angles at:
- o Span 5, stringer 3 connection to FB 3
- o Span 7, stringer 1 connection to FB 0
- o Span 7, stringer 3 connection to FB 0
- Monitor welded connections at recently replaced FBs.

ſ	NBI No.:	Structure No.:	Local ID:	Suff. Rating:	ND
l	17611	5159 0300 X	-1	66.70	ND

ELEMENT CONDITION STATE DATA

Elem. / Env	Description	Unit	Total Qty	% 1	Qty. 1	% 2	Qty. 2	% 3	Qty. 3	% 4	Qty. 4	
12 / 1	Re Concrete Deck	sq.ft	53,984.00	0%	0.00	100%	53,984.00	0%	0.00	0%	0.00	

PX – Minor to moderate debris along curbs. The deck scupper in span 10 near pier 10 is clogged. Several additional scuppers are partially clogged with vegetation.

Isolated shallow spalls exist in the deck.

Longitudinal cracks exist along the deck surface, mostly in the wheel lines.

Transverse cracks spaced at 1 to 3 feet exist on the surface randomly along the full length of the bridge. Cracks are widest and most prominent in the twin girder spans.

Deck patches exist from a prior rehabilitation. The deck patches are functioning as intended.

Note: The deck is being coded CS2 (Soffit CS3) due to areas of the deck being visible due to the deterioration of the wearing surface.

	Treater the desired sering season serious of the desired straining the desired and to the desired action of the free model and the desired serious straining serious serious serious straining serious											
510 / 1	Wearing Surfaces	sq.ft	53,984.00	60%	32,391.00	35%	18,894.00	5%	2,699.00	0%	0.00	
	Epoxy grit overlay (installed 2014) failing in patches throughout the deck, mostly along the wheel lines.											
107 / 1	Steel Opn Girder/Beam	ft	4,780.00	82%	3,900.00	10%	478.00	8%	402.00	0%	0.00	

Fracture Critical twin girder spans exist in spans 5 through 7 and have the following comments:

Cracks at horizontal web splice terminations at:

PX – Span 5, G 1 near FB 5 – 5/8 inch, not arrested.

FX - Span 5, G 2 near FB 5 - 3/8 inch (likely paint crack).

FX – Span 6, G 1 near FB 3 – 3/4 inch, arrested with two holes.

PX - Span 6, G 2 near FB 11 - 3/16 inch, not arrested.

FX - Span 7; G 1 near FB 4 - 1 inch and 1 1/8 inch (likely paint cracks) in girder web at toe of longitudinal stiffener.

FX – Span 7; G 2 near FB 4 – Two vertical cracks arrested with drilled hole retrofits.

PX – Missing or loose bolts at:

Span 5, G 2 near FB 5.

Span 6, G 1 top interior top flange.

Span 6, G 1 interior face horizontal splice at pier 6

Span 6, G 2 exterior face top and bottom flanges near FB 3.

Span 6, G 2 exterior face horizontal splice near FB 12.

Span 7, G 1 exterior face horizontal splice near FB 3.

FX – A global bow up to 1/2 inch exists in the web of G 1; span 7 between FB 3 and 4 at the field splice.

1/8-inch pack rust between top flanges and deck is common.

FX - Cracks (retrofitted) at longitudinal stiffener butt welds at:

Span 5; G 1 between FB 4 and 5. A paint crack has formed along the girder web.

Span 6; G 1 near FB 6

Span 6; G 1 near FB 7

Span 6; G 1 near FB 9

Span 6; G 2 near FB 9

Span 7; G 2 between FB 7 and 8

Painted over pitting was observed in the web of the girders adjacent to the top of lower lateral bracing gusset plates.

Pack rust (1/2 inch) between horizontal web splice causing distortion at several locations.

Pack rust (5/16 inch) at bottom flange splice plates.

Heavy laminating corrosion was noted at the girder horizontal web splices at the bearing stiffeners over piers 5 and 6. G 2 over pier 6 also has up to 50% section loss to 4 of 6 bolts.

Pack rust (3/16 inch) in girder top flange at deck joints.

One missing bolt was noted at the FB 2 connection to G 1; span 7.

Multi girder spans exist in spans 1 through 4 and 8 through 15 and have the following comments:

FX – Isolated CF top struts exhibit cracked welds between the CF and gusset plate due to pack rust. The following locations exhibited cracks:

CF at pier 1 to G 3 - 5 3/8 inch.

CF at pier 3 to G 4 - 1/4 inch.

CF at pier 4 to G 1, span 4 - 1/4 inch.

CF at pier 12; connection to G 2 - full length of gusset plate.

Pack rust (1 1/4 inches) typical between CF members and vertical web stiffeners. Minor to moderate pitting and distortion to the gusset plate also present at these locations.

Girder cross frames between G 1; 2 and 3 at pier 9 and pier 10 exhibits a 3-inch bow, most likely due to the bearing rehabilitation project.

Vertical crack (1 3/4 inch) in bearing stiffener fillet weld at exterior face of G 1, span 15 at pier 14.

515/1	Steel Protective Coating	sq.it	140,000.00	0%	0.00	100%	140,000.00	0%	0.00	0%	0.00	
	Painted in 2010. Areas of previous co	rrosion	and pack rust a	re reacti	vating in ma	iny locat	ions especial	ly at guss	set plates ne	ar the		
	expansion joints. Pack rust is active ir	many	girder horizonta	al web sp	lices. Previ	ous PX o	of laminating	corrosion	and pack ru	ust at		
	lower lateral bracing gusset plates wer	e repai	ed prior to the	2014 OS	although co	orrosion	is reactivating	g in isolat	ed locations	5.	_	
113 / 1	Steel Stringer	ft	1,914.00	97%	1,850.00	3%	50.00	1%	14.00	0%	0.00	

	NBI No.:	OKIANOMA DE	•		Local ID:		•	Rating:		
	17611	5159 030			-1		·	66.70		ND
				and FD				00.7U		
	PX – Loose stringer conn Span 5, stringer 2 at FB		mnection angle	and Fb wei	b at.					
	Span 5, stringer 3 at FB									
	Span 5, stringer 3 at FB									
	Span 6, stringer 1 at FB									
	Span 6, stringer 2 at FB									
	Span 6, stringer 3 at FB									
	Span 6, stringer 1 at FB									
	Span 6, stringer 1 at FB									
	Span 6, stringer 2 at FB									
	Span 6, stringer 3 at FB									
	Span 6, stringer 3 at FB									
	Span 6, stringer 1 at FB	11 – 5 loose bolts								
	Span 6, stringer 1 at FB	12 – 1 loose bolt								
	Span 7, stringer 3 at FB	4 – 1 loose bolt								
	Multiple stringers have mi	s-drilled holes in botton	n flange at FB o	connections	<u> </u>					
152 / 1	Steel Floor	Beam ft	891.00	57%	508.00	200.00	21% 1	83.00 0%	0.00	
	The FBs in spans 5 throu	gh 7 act as trusses.						<u> </u>		
	PX – FB 6; span 5 at G 1	has 5 1/8-inch crack in	weld for upper	connection	plate.					
	PX – FB 0; span 6 at G 2					d.				
	PX - Span 5; west face o	f FB 6 at G 1, weld for t	he web connec	tion plate cr	acked 4 1/2 ir	nches.				
	PX – Loose and misaligne	ed bolts exist in the FB	to G connection	ns at severa	l locations.					
	FX – FBs replaced at FB									
	Previous repair to FB 0 at	•		d plate and	has 1 1/8-inch	n and 1/2-inch cra	acks in welds.			
	Several kinks and bends	•	•							
	Span 6, U3L2 of FB 2 has				-					
	FB 4; span 6 exhibits two		•	under string	er 3.					
	Oversized holes exist ran									
	Span 6, FB 6 top flange h	•		-	knife edging.					
	Several FBs exhibit surface	• .	•							
	Corrosion of flanges and	1/8 inch pitting on botto	m race or top ri	ange.						
	ELOOD DDAOING CVCT	-M								
	FLOOR BRACING SYST		· :		-4 -1-4-					
	PX – Span 5 LLB at G 2;			-	-					
	PX – Span 6 LLB at G 2;				•					
	LLB hanger rods are seve Span 6 LLB between FBs	•	•							
	A 5-inch by 2-inch corrosi		_	_		stiffener to G 1:	span 7			
205 / 1	Re Conc C			88%	·	0% 0.00	12%	3.00 0%	0.00	
20571	North column of pier 4 ex				20.00	0.00	1270	0.00	0.00	
	Column of pier 6 exhibits	•			scence and fu	ll width snalling v	vith exposed r	ainforcement at t	·he	
	cross-section change nea	•	cai cracks with	iigiit eiliores	scence and id	ii widiii spaiiiig v	vitii exposed ii	simorcement at		
	North column of pier 8 ex		th exposed rein	forcement						
215 / 1	Re Conc Ab		80.00	0%	0.00	78.00	3%	2.00 0%	0.00	
213/1	E abutment slope protecti									
	observed.	on covered in vines and	a vegetation. T	THE DOLLOTTIC	n trie abutiliei	ii bieasiwali is e.	xposed due to	prior erosion, no	plies	
	Bottom of breastwalls at b	ooth abutments are evn	osed up to 2 in	chee hiah a	nd 1 feet wide	at ends with un	to 30 inches o	f nenetration		
	Both abutments appear to	-		_		-			ement	
	from soil pressure acting	•	Jonamie, DUII	, apauliciils	, are supporte	a on vertical pile	o windi ale su	cochable to IIIOV	omont	
	The east abutment exhibi		d area hetween	girders 2 a	nd 3 and a ho	rizontal crack wit	h rust staining	near the girder	3	
	pedestal.		JOU DOLWOOII	5" 4015 £ al		ontar order wit	doc otali ili ig	sai alis giraei	-	
234 / 1	Re Conc P	ier Cap ft	594.00	71%	424.00	20% 120.00	8%	50.00 0%	0.00	
	Pier 1 - Spall in edge nea							3.3		
	Pier 2 - 3/16-inch crack al	•	es near G 2 wit	h adiacent (delamination i	n top face				
	Pier 3 - 1/16-inch cracks	· ·		•		•	spalls with evr	osed reinforcing	in the	
	west face.	and top lace with larg	jo dolaminated	a. 040. 1116	wali ildə	manipio silaliow	opano with exp	Joseph Tell Horolling	, u.o	
	Pier 4 - spalls and scaling	exposing corroded rein	nforcina steel ir	the bearing	n seat areas a	nd in west face o	ver north colu	mn· Scaling (1/8	inch	
	deep) around G 1 bearing			bearing	, Jour urous a	III WOOL IAGE C		, Soaming (1/0		
	Pier 5 - West face at inter		xhibits multiple	exposed an	d corrodina re	einforcina steel er	nds : random h	airline shrinkage	cracks	
	and isolated areas of sma		ono manipie (capooou all	Jon Journy 10	g steel el	.ao , randoni i	Similkaye		
	Pier 7 - map cracks in the		alling with expo	sed reinforc	ement around	the base of port	h column			
	Pier 8 - 1/16-inch x 5-foot	·	• .					te. Cracking and	l	
	delaminations are due to	-	-	or	J 4. 9 1 41					
	Pier 13 - longitudinal crac		•	<u>)</u>						
	Pier 14 - 1/16-inch cracks				and scaling	concrete with exp	osed corroded	d reinforcina stee	el exists	
	in the bearing seat areas				,		55.10400	5. 5ig 5.00		
310 / 1	Elastomeric		12.00	100%	12.00	0.00	0%	0.00 0%	0.00	
J 10 / 1	Previous rocker bearings								L 3.00	
			_						0.00	
044 1 1	Moveable E	Bearing each	n 30.00	0%	0.00	26.00	13%	4.00 0%	0.00	
311 / 1	Table 10 Comments	to a contract to the first								
311 / 1	Typically exhibit rust stain	-	-							
311 / 1	Keeper plates broken free	e or have cracked welds	s at sole plate fo	or G 3 and C	G 4 at west ab	outment.				
311 / 1	• • •	e or have cracked welds tated about vertical axis	s at sole plate for s with SW corne	or G 3 and C	G 4 at west ab ing mason <u>ry p</u>	outment.	7%	2.00 0%	0.00	

					JL. OI 118	3110poi			3	<u> </u>				
		<u> </u>	_	ucture N			Local I	<u>D:</u>		<u>s</u>	uff. Ratin			ND
	1	7611	515	9 0300	X		-1				66.70			
		Bearing anchor bolts are lo			• .	•		iple location	ons.					
204 / 4	Турі	cally exhibit surface corrosion		_				E00/	1.00	00/	0.00	00/	0.00	
321 / 1	Dath	Re Conc Approach		sq.ft	2.00	50%	1.00	50%	1.00	0%	0.00	0%	0.00	
		n approach slabs have been oall measuring 2 feet by 6 in	•	•		•	o exhibits t	ıp to 0.02t	inch wide	ongituaina	ai cracking	in the wi	ieei iiries.	
330 / 1	ДЭР	Metal Bridge Railir		ft	3,856.00	95%	3,651.00	5%	200.00	0%	5.00	0%	0.00	
00071	PX -	– Easternmost rail post alon												
		lls exist in the sidewalk of sp					•		3					
	Wes	st termination of the north br	idge rail is	missing	one rail post	and multip	le blockout	s of the no	ortheast ap	proach raili	ing are twi	sted / da	maged.	
		th bridge rail in span 7 near				•	steel tube.							
040 /		oan 10; the south metal rail			_		0.00	1000/	0.260.00	00/	0.00	00/	T 0.00	
919 /		St.(Rail) Prot. Coa		sq.ft	9,260.00	0%	0.00	100%	9,260.00		0.00	0%	0.00	
		Isolated areas of the painter	•		•	ibit peeling	paint due	to adhesio	n failure b	etween the	top and in	termediat	te	
331 / 1		coats. Areas of corrosion ar Re Conc Bridge Rai		ft ft	3,856.00	100%	3,856.00	0%	0.00	0%	0.00	0%	0.00	
331/1	The	steel bridge railing has rece											L	
		exhibit minor cracking.	only been	pairiteu	and the conci	ete briage	railing nas	recently b	CCII SKIIII	coateu. Isoi	ateu areas	o or the oc	Jilorete	
		or debris exists along the to	e of both th	he north	and south ba	rriers.								
	The	curbs exhibit active vertical	cracks an	d small s	spalls with exp	oosed reinf	orcing due	to insuffic	ient cover					
	Tape	ered concrete curbs have be	en installe			-							-	
859 / 1		Soffit		each	1.00	0%	0.00	0%	0.00	100%	1.00	0%	0.00	
		- Isolated spalls, 4 to 6SF a	•				•							
		- Shallow spalls common al	ong top tia	inge of g	irders, floor b	eams, and	stringers.	isolated lo	cations na	ve spalls up	1001 1 00	wide with	exposea	
		oding reinforcing steel. k lifting from girders and floo	or heams a	at isolate	d locations di	ie to nack i	ruet							
		tiple 1/4-inch-wide cracks ex						n 6 where	stringers a	are not cont	inuous ove	er FBs.		
		nsverse cracks with effloreso										50.		
		nkage and hairline map crac		-				3		•				
	Man	y scuppers in the main spar	ns are fille	d with fo	am installed o	luring the r	ecent deck	overlay ir	stallation.					
865 / 1		St.Open Gird End(5	5Ft	ft	180.00	78%	140.00	22%	40.00	0%	0.00	0%	0.00	
		ve corrosion was noted at th	•		•		•							
	Pac	k rust and section loss up to		T .			_				0.00	00/	T 0.00	
870 / 1		Concrete Wingwa	lll .	each	4.00	100%	4.00	0%	0.00	0%	0.00	0%	0.00	
	NO S	significant deficiencies.	14		1 000 00	7.40/	000.00	00/	400.00	100/	040.00	00/		
872 / 1	D	St.Gird Und Const		ft	1,236.00	74%	920.00	8%	100.00	18%	216.00	0%	0.00	
	Pac	k rust and laminating corros			_		00.00	00/	0.00	00/	0.00	00/	0.00	
877 / 1	N 1.	St. Stringer End(5F	-τ)	ft	30.00	100%	30.00	0%	0.00	0%	0.00	0%	0.00	
	NO S	significant deficiencies.	14	_ A	200.00	4000/	200.00	00/	0.00	00/	0.00	00/	T 0.00	
879 / 1	ΓV	St.Strng.Un Const.		ft	300.00	100%	300.00	0%	0.00	0%	0.00	0%	0.00	
		– Stringer connetion angle w an 5, stringer 3 at FB 3 – 3												
		an 7; stringer 1 at FB 0 – 1												
		an 7; stringer 3 at FB 0 – 1												
		ortion of stringer 3; at FB 0;		s been re	e-sectioned.									
906 / 1		Sealed Exp.Jt.(SE.	J-3	ft	105.00	0%	0.00	100%	105.00	0%	0.00	0%	0.00	
		led expansion joints at the v		nent, and	l over piers 10	and 14 ha	ave been r	eplaced ar	nd have m	oderate deb	ris impact	ion. Seale	ed	
	eyna	ansion joints are all nearly c	losed.		_			T = e = : T		1				
	СХР	a. =/	_	-			0.00	50%	35.00	50%	35.00	0%	0.00	
907 / 1	Ċ	St.Finger Jt. (SED		ft	70.00	0%							_	
907 / 1	Pier	4 finger joint exhibits mode	rate debris	s impacti	∟ on along with	a slight ve	rtical offse		3/8 inch h				_	
907 / 1	Pier	4 finger joint exhibits mode embly. Two 5-foot sections of	rate debris	s impacti 4 finger j	_ on along with joint have bee	a slight ve en replaced	rtical offse with a we	ded steel	3/8 inch h plate.				_	
	Pier	4 finger joint exhibits mode embly. Two 5-foot sections of finger joint exhibits mode	rate debris of the pier rate debris	s impacti 4 finger j s impacti	on along with joint have bee	a slight ve en replaced a slight ve	rtical offse with a we rtical offse	ded steel of 1/8 inc	3/8 inch h plate. ch.	igher from t	he west as	sembly to	o the east	
907 / 1	Pier asse Pier	4 finger joint exhibits mode embly. Two 5-foot sections of 7 finger joint exhibits mode Pourable Fix Jt.Se	rate debrisof the pier rate debrisonal	s impacti 4 finger j s impacti ft	on along with joint have been along with 1,890.00	a slight ve en replaced a slight ve	rtical offse with a we rtical offse 150.00	ded steel of 1/8 inc	3/8 inch h plate. ch. 1,040.00	igher from t	he west as	sembly to	_	
	Pier asse Pier	4 finger joint exhibits mode embly. Two 5-foot sections of finger joint exhibits mode Pourable Fix Jt.Se	rate debris of the pier rate debris al ts have m	s impacti 4 finger j s impacti ft oderate	on along with joint have bee on along with 1,890.00 debris impact	a slight ve en replaced a slight ve 8%	rtical offse with a we rtical offse 150.00 ded seals,	ded steel of 1/8 ind 55% and a few	3/8 inch h plate. ch. 1,040.00 shallow s	igher from to 37% on the control of	he west as 700.00 atches in he	0% eaders.	0.00	
	Pier asse Pier FX -	4 finger joint exhibits mode embly. Two 5-foot sections of finger joint exhibits mode Pourable Fix Jt.Se Joint seals at the abutmen red seal deck control joints.	rate debris of the pier rate debris al ts have m are space	s impacti 4 finger s impacti ft oderate d at 18 fe	on along with joint have bee on along with 1,890.00 debris impact eet in approact	a slight veen replaced a slight veen 8% con, debond	rtical offse with a we rtical offse 150.00 ded seals, nd 50 to 75	ded steel of 1/8 ind 55% and a few	3/8 inch h plate. ch. 1,040.00 shallow s	igher from to 37% on the control of	he west as 700.00 atches in he	0% eaders.	0.00	
909 / 1	Pier asse Pier FX -	4 finger joint exhibits mode embly. Two 5-foot sections of finger joint exhibits mode Pourable Fix Jt.Se	rate debris of the pier rate debris eal its have mare spaced acking and	s impacti 4 finger s impacti ft oderate d at 18 fe	on along with joint have bee on along with 1,890.00 debris impact eet in approact	a slight veen replaced a slight veen 8% con, debond	rtical offse with a we rtical offse 150.00 ded seals, nd 50 to 75	ded steel of 1/8 ind 55% and a few	3/8 inch h plate. ch. 1,040.00 shallow s	igher from to 37% on the control of	he west as 700.00 atches in he	0% eaders.	0.00	
	Pier asse Pier FX - Pou and	4 finger joint exhibits mode embly. Two 5-foot sections of finger joint exhibits mode Pourable Fix Jt.Se Joint seals at the abutmen red seal deck control joints the joint headers exhibit crass.	rate debris of the pier rate debris eal ts have m are spaced acking and	s impacti 4 finger s impacti ft oderate d at 18 fe spalls p each	on along with ioint have been along with 1,890.00 debris impact eet in approact atched with control 12.00	a slight ve en replaced a slight ve 8% ion, debond spans ar oncrete and 100%	rtical offse with a we rtical offse 150.00 ded seals, and 50 to 75 d asphalt. 12.00	ded steel of 1/8 inc 55% and a few feet in the	3/8 inch h plate. ch. 1,040.00 shallow s e main spa	37% and pains. Joint se	700.00 atches in heals exhibit	0% eaders. areas of	0.00 failure	
909 / 1	Pier asse Pier FX - Pou and	4 finger joint exhibits mode embly. Two 5-foot sections of finger joint exhibits mode Pourable Fix Jt.Se Joint seals at the abutmen red seal deck control joints the joint headers exhibit craft.	rate debris of the pier rate debris cal ts have m are space acking and bly an 4 at pie	s impacti 4 finger s impacti ft oderate d at 18 fe spalls p each	on along with ioint have been along with 1,890.00 debris impact eet in approact atched with control 12.00	a slight ve en replaced a slight ve 8% ion, debond spans ar oncrete and 100%	rtical offse with a we rtical offse 150.00 ded seals, and 50 to 75 d asphalt. 12.00	ded steel of 1/8 inc 55% and a few feet in the	3/8 inch h plate. ch. 1,040.00 shallow s e main spa	37% and pains. Joint se	700.00 atches in heals exhibit	0% eaders. areas of	0.00 failure	

		(Oklahoma	a Dept.	of Tra	ansport	ation -	Brid	ge Ins	spectio	n Rep	ort				
		l No.:		ucture No.	_		Local ID:			Sı	uff. Ratin	<u>g:</u>				ND
		7611		59 0300 X			-1				66.70					
		N SPAN TWIN GIRDE														
		cks at horizontal web s – Span 5, G 1 near F	•													
		- Span 5, G 1 near F	,													
		- Span 6, G 1 near F	•		,	S.										
	PX	- Span 6, G 2 near Fl	B 11 – 3/16 inch	, not arreste	ed.											
		- Span 7; G 1 near F					-	at toe of	longitudin	ıal stiffener.						
		- Span 7; G 2 near F				h drilled hole	retrofits.									
		- Cracks (retrofitted) a an 5; G 1 between FB	•			ona the airde	er web									
		an 6; G 1 near FB 6	. aa o. /.pa			og g a.										
	Spa	an 6; G 1 near FB 7														
		an 6; G 1 near FB 9														
		an 6; G 2 near FB 9	7 0 1-													
	Sp	an 7; G 2 between FB	7 and 8web.													
	APP	ROACH SPAN MULT	I GIRDERS													
	Vert	cal crack (1 3/4 inch)	in bearing stiffe	ner fillet wel	ld at exteri	or face of G	1, span 15	at pier 1	4.							
	FI O	OR BEAMS														
		- FB 6; span 5 at G 1	has 5 1/8-inch c	rack in welc	d for upper	connection p	olate.									
	PX -	- FB 0; span 6 at G 2	cracked full leng	gth of botton	n weld and	full height o	f vertical w	eld.								
	STR	INGERS														
		- Stringer connetion a	ngle weld cracks	s at:												
		an 5, stringer 3 at FB	-													
		an 7; stringer 1 at FB		;												
	Sp	an 7; stringer 3 at FB	0 – 1 inch.													
	CRC	SS FRAMES														
		- Isolated CF top strut		d welds betv	ween the C	CF and gusse	et plate due	to pack	rust. The	following lo	cations ex	chibited o	crack	s:		
		at pier 1 to G 3 – 5 3/														
		at pier 3 to G $4 - 1/4$ at pier 4 to G 1, span														
		at pier 12; connection		ngth of guss	et plate.											
	FI 0		-14													
		OR BRACING SYSTE - Span 5 LLB at G 2; e		7 has 5-inch	crack in w	veld to ausse	t plate									
		- Span 6 LLB at G 2;				-	-) .								
957 / 1		Pack Rust Sn	nart Flag	each	1.00	0%	0.00	0%	0.00	100%	1.00	0%		0.00		
		Pack rust is causing	cracking of con	nection weld	ds for floor	beams guss	et and con	nection	olates, stri	nger connec	ctions and	lower la	teral			
	brac	ing. < rust developing betw	veen holted hori:	zontal web s	enlice in m	ain airdere (s	nane 5-7)	and hott	om flance	enlica nlata	e in main :	and ann	roach	,		
		er spans.	veen boiled non.	Zoniai wob .	opiloc ili ili	ani giracis (c	pans o-r)	and bott	om nange	opiloc plate	3 III III GIII (ана аррі	loadi	•		
958 / 1		Concrete Cra		each	1.00	0%	0.00	0%	0.00	100%	1.00	0%		0.00		
		gitudinal cracks exist a	•		•		bridge C-	noke er-	widest s-	d most se-	minant in 4	ho tuin :	nirds.	-		
	spar	sverse cracks exist or ns.	n die sunace fal	ndoniny alon	ıy une iuli le	zilgul ol the l	onage. Cr	acks are	widest an	u most pror	mnent in t	iie iwin (yıı uel	1		
		iple 1/4-inch wide crac	cks exist along t	he stringer	deck haun	ch at locatior	ns in span 6	where	stringers a	re not conti	nuous ove	r FBs.				
		deck soffit exhibits rai		e cracking w	vith efflores	scence throu	ghout. Th	e crackir	ng is heavi	est within 3	FBs/diaph	ragms o	of the	piers		
		is typically spaced at a nkage and hairline ma		mmon thro	iahorit											
960 / 1	J. 11 1	Settlemer	·	each	1.00	0%	0.00	0%	0.00	100%	1.00	0%		0.00		
		abutments appear to	•	ards the cha	annel base	d on measur	ements be	ween ba	ackwall an	d girder flan	iges. Diffe	erence b	etwe	en		
		and bottom flange clea														
		abutment = 2 1/8 inch abutment = 2 1/8 inch														
963 / 1		Steel Section		each	1.00	0%	0.00	100%	1.00	0%	0.00	0%	T	0.00		
	Pain	ted over pitting was o		veb of the g	irders adja	cent to the to	pp of lower	lateral b	racing gus	set plates.						
		top flange in span 6		-		-										
969 / 1	A 5-	nch by 2-inch corrosion		rough LLB (gusset plat 1.00	te at the edge	e of the FB 0.00	6 stiffer	ner to G 1, 1.00	span 7.	0.00	0%		0.00	_	
JUJ / 1		Caton lane b		00011	1.50		0.00	.0070	1.00	J 70	0.00	U 70		0.00		

NBI No.:	Structure No.:	Local ID:	Suff. Rating:	ND
17611	5159 0300 X	-1	66.70	ND

FX - Global 1/2-inch bow in web of G 1, span 7 between FBs 3 and 4 at the field splice.

FX – Several kinks and bends were noted in floor beam members and gusset plates. Locations:

FB 5; span 5 at G 2; L4 gusset plate - bow.

FB 2; span 5 at G 2; L4 gusset plate - bow.

FB 7; span 5; adjacent to G 2 - 3/8-inch kink in the U3 gusset plate under stringer 3 and approximately 1/8-inch bow in the L4 gusset plate.

FB 4; span 6 center gusset plate kinked.

FB 13; span 6 at L0L1 – exhibits 2 minor kinks.

FB 1; span 7 at stringer 3 – bottom flange of the upper chord is twisted to the east. The upper gusset plate under stringer 3 is kinked 1/2 inch on the vertical edges and 1/2 inch on the bottom horizontal edge. Vertical stiffeners are out of alignment. The center gusset plate is kinked 1/4 inch to the west.

FB 2; 5 and 8 in span 7 at stringer 3 – a 1/4-inch kink in the bottom horizontal face of the gusset plate and rotated up to 1/2 inch to the west. Poor weld quality exist between the north vertical stiffener under stringer 3 and FB 2 bottom flange.

Span 6; LLB has up to 1 inch of pack rust between the gusset plate and the floor beam causing the bracing to rotate.